

Lock-in amplifier

Introduction:

http://www.signalrecovery.com/_AppsNotes/TN1007.pdf

Refresh: Synchronous Detection (Sensors and Transducers):

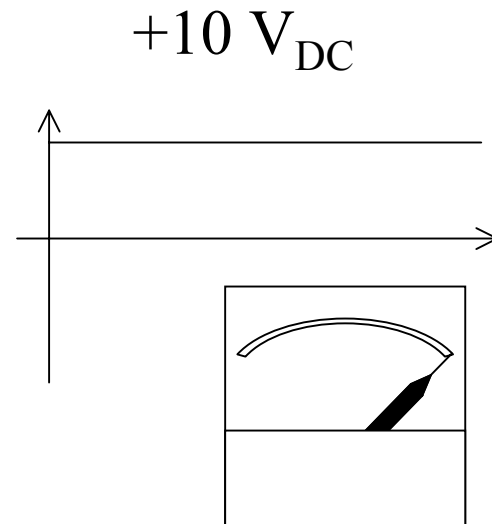
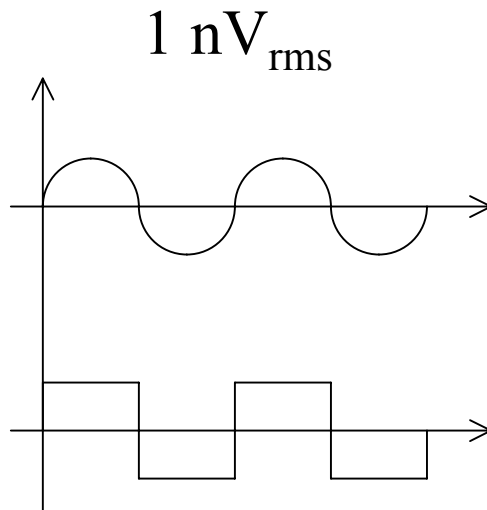
<http://measure.feld.cvut.cz/system/files/files/cs/vyuka/predmety/A3M38MSZ/SynchrDetectBW.pdf>

LIA Key parameters

- Full-scale sensitivity
 - Synchronous input sine RMS ($\mu V_{rms} \sim \pm 10 V_{dc}$)
- Linearity and Out-of-phase rejection
 - Maximum asynchr. signal causing distortion $<$ limit
- Dynamic reserve – defined as
 - Out-of-phase rejection ratio for distortion $< 5\%$
 - Or simply as ratio of full scale signal to clipping level
- Output stability and drift
- LP filter parameters

Full-scale sensitivity

- RMS value of *synchronous* input sinewave giving *Full scale output* (typ. 10Vdc)
- Ex.: $S_D = 1 \text{ nV} \dots \text{Output} + 10 \text{ V}$



Linearity and Out-of-phase rejection

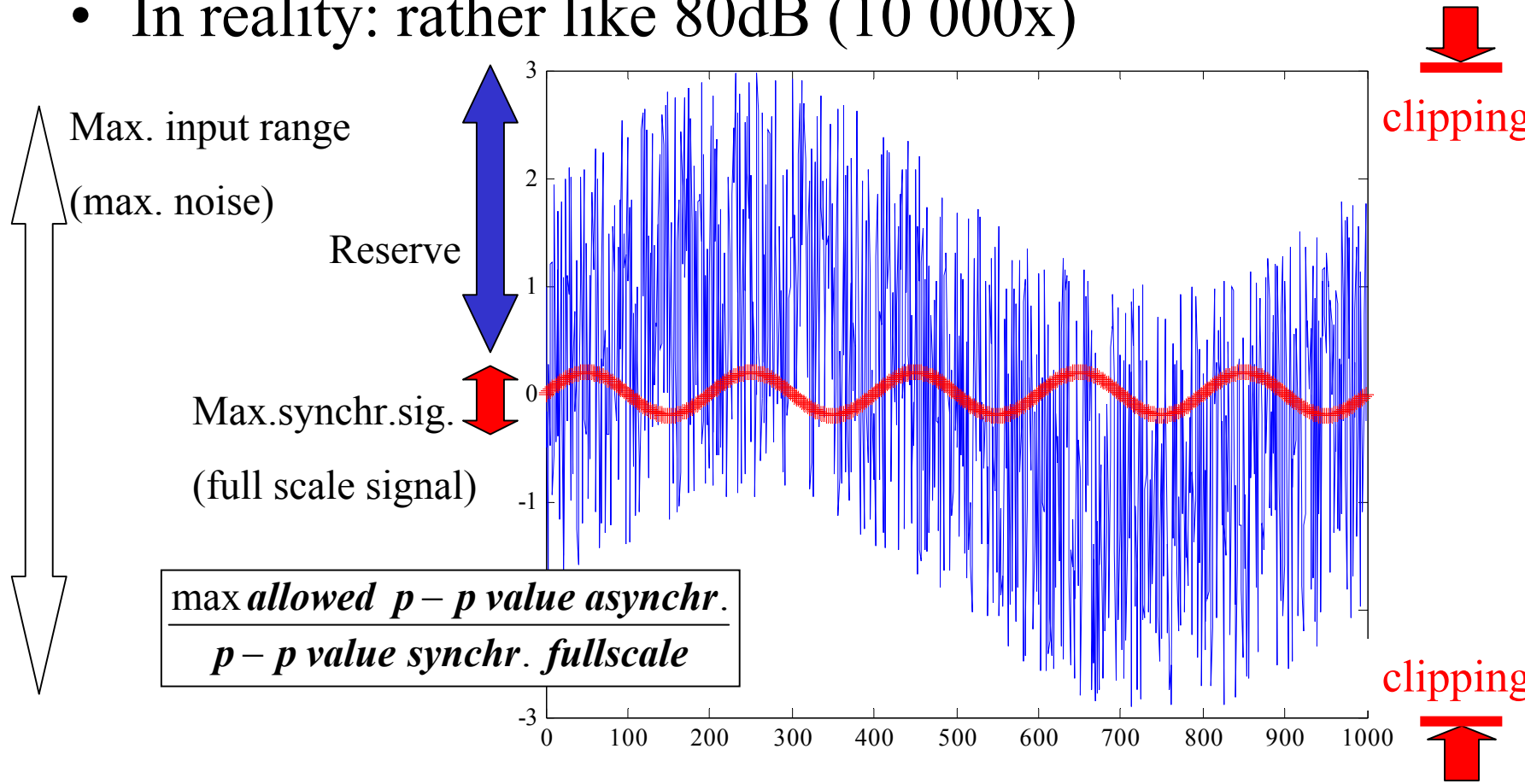
- =Maximum asynchronous signal causing distortion < limit
- Theoretically (linear): no sensitivity to asynchr. signal
- Practically: high noise (below clipping level) -> some influence on output
- (Noise *above* clipping level -> gross errors)
- Out-of-phase rejection = ratio of:
 - synchr. (sine) signal ~ full scale
 - asynchronous (sine) signal: maximum amplitude causing change < (say) 1%

$$\frac{\text{rms value asynchr.}}{\text{rms value synchr. fullscale} \cdot 1\%} \approx \frac{1\,000\,nV}{1\,nV \cdot \frac{1}{100}} \approx 100\,000\times \approx 100dB$$

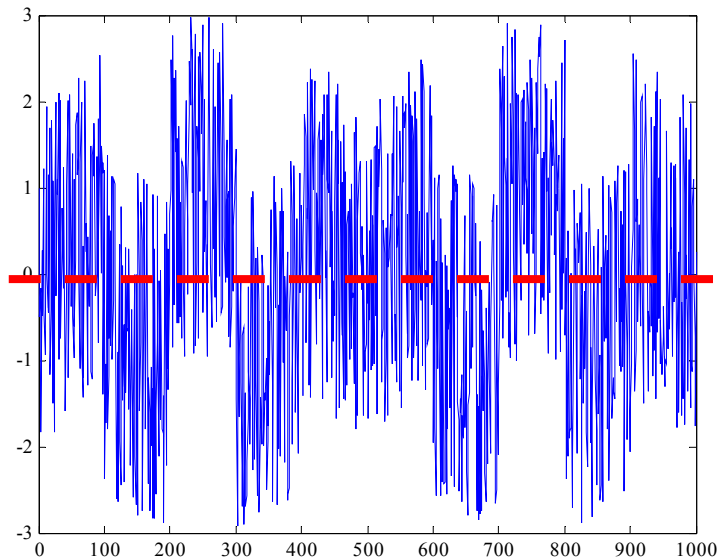
- Linearity: also main reason to use switching SD (rather than analog multiplier)

Dynamic reserve

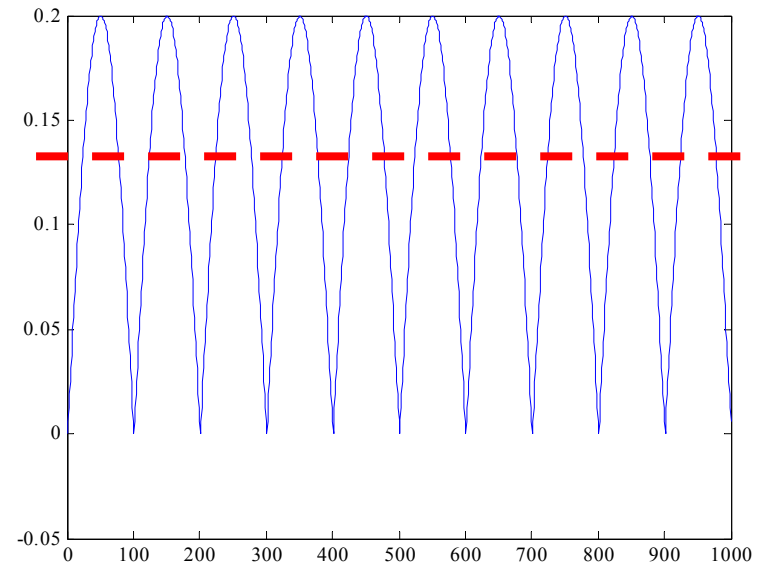
- Max. synchronous signal vs. Max. tolerable noise
- In reality: rather like 80dB (10 000x)



Syn. detected noise and signal



Mean = -0.0029



Mean = 0.1273

← Output (LF) gain 1x → 10x ... Dynamic reserve + 10x = +20dB

Ex.: $S_D = 1\text{mV}_{\text{rms}} \approx 3\text{mV}_{\text{pp}}$, clipping 3V \Rightarrow D.R. = 1000x = 60dB

Output Expand 10x:

$S_D = 0.1\text{mV}_{\text{rms}} \approx 0.3\text{mV}_{\text{pp}}$, clipping 3V \Rightarrow D.R. = 10 000x = 80dB

Output stability and drift, Minimum detectable signal

- LIA output: DC offset (teoretically 0, practically compensated – [AUTO OFFSET]) *Note: +/-180°*
- Drift („output stability“): e.g. 100 ppmFS / K
- Minimum detectable signal:
- $S_{\min} = 100\text{ppm} \times 100 \text{ nV} = 0.01\text{nV}$

$$s_{\min} = \delta \times S_D$$

Output expand 10x => + 10x D.R. ☺
- 10x s_{\min} ☹

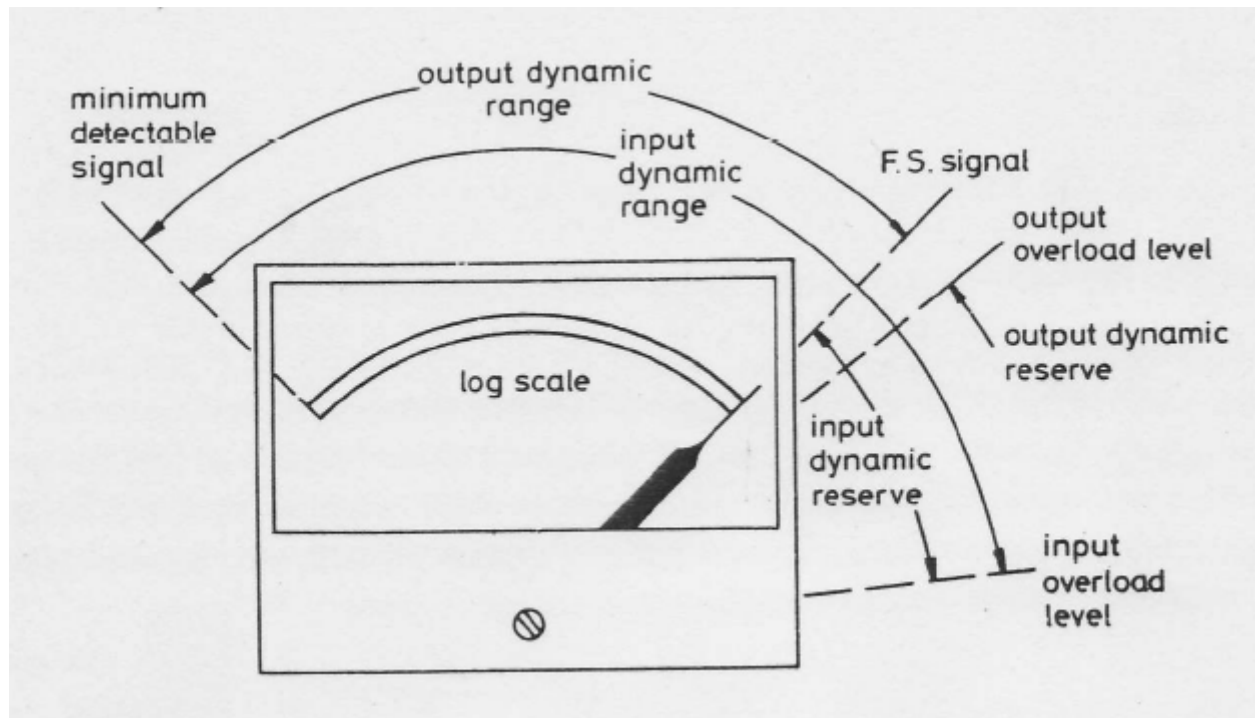
(input) Dynamic range

- Not Dynamic *reserve*
- Maximum voltage swing / minimum detectable signal

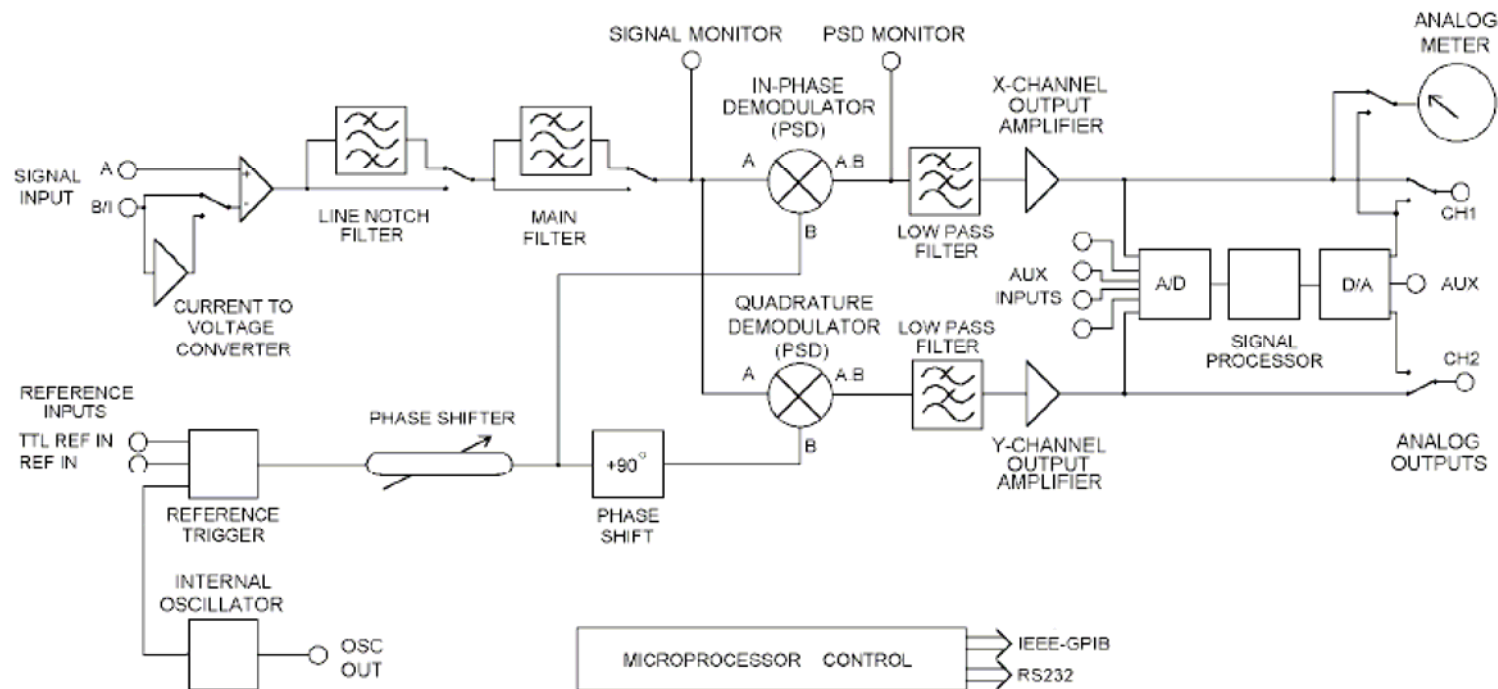
$$D_I = \Delta v / s_{\min}$$

- Δv = dynamic reserve x S_D
- $s_{\min} = \delta \times S_D$
- $\Rightarrow D_I = \text{dynamic reserve} / \delta$
- Ex.: $D_I = 1\,000 / 100 \text{ ppm} = 10^7 = 140\text{dB}$

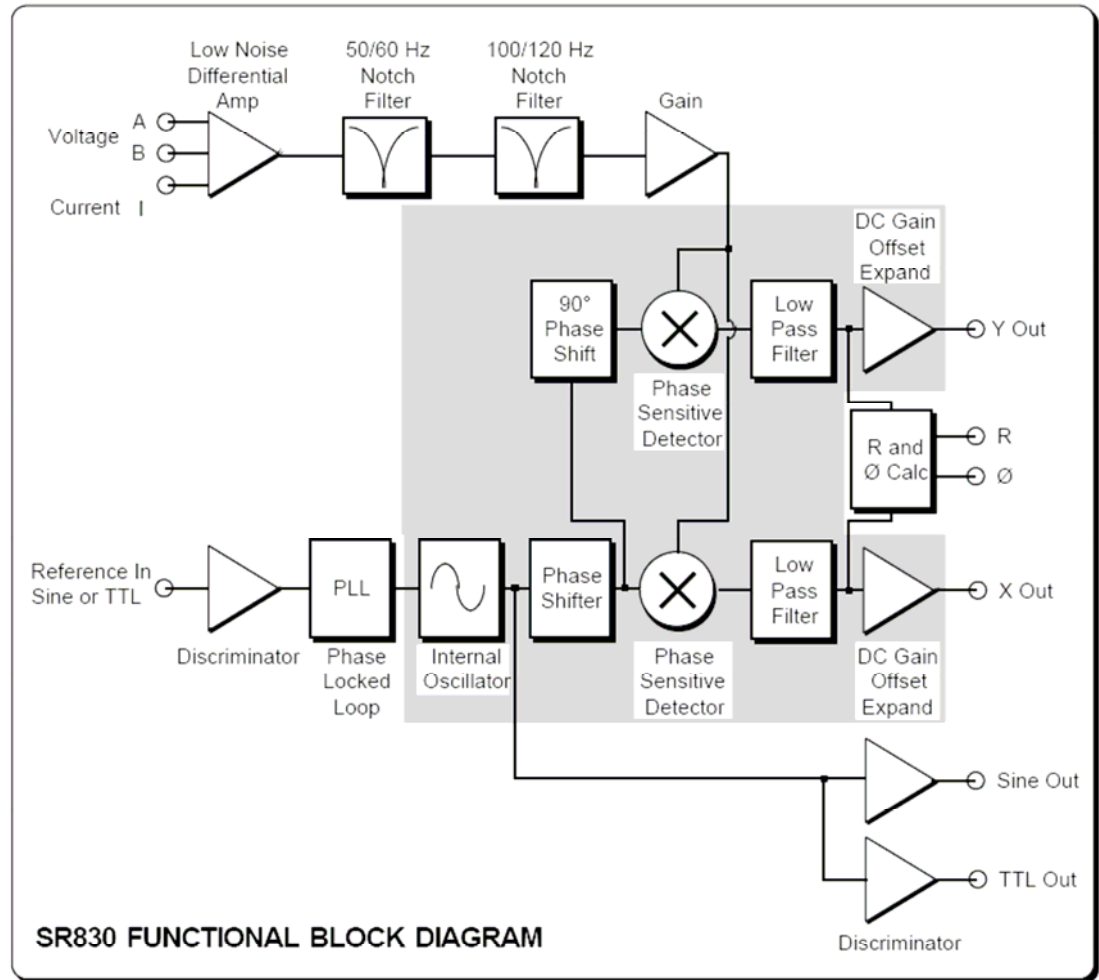
LIA Parameters



Analog LIA - EG&G 5210



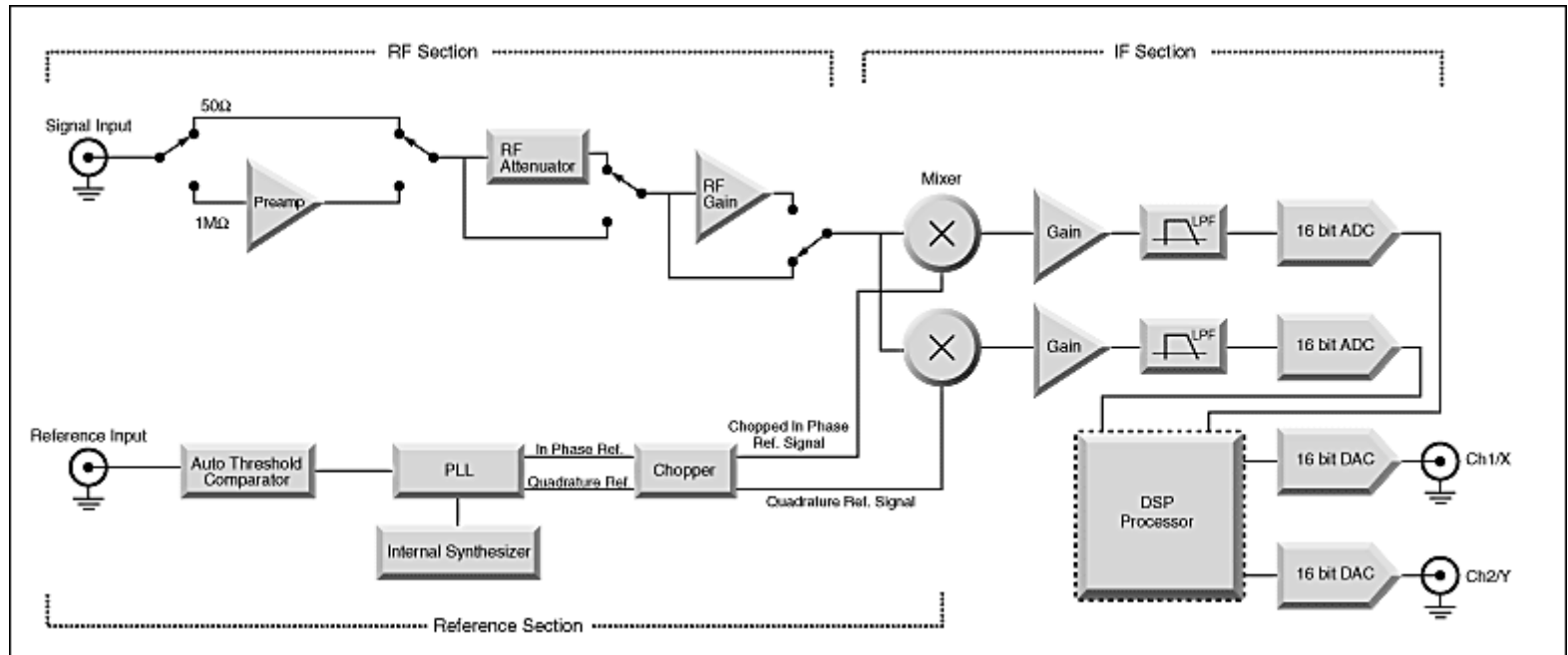
DSP LIA – SR830



Stanford Research Systems

<http://www.thinksrs.com/products/SR810830.htm>

RF (200MHz) LIA – SR844



What is it good for?

- Signal spectra transposition via modulation
 - Avoiding noisy bands
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- Note: spread spectrum modulation, CDMA