

Innovative LED Solutions



PRODUCT SELECTION GUIDE LED Lighting Reference Designs

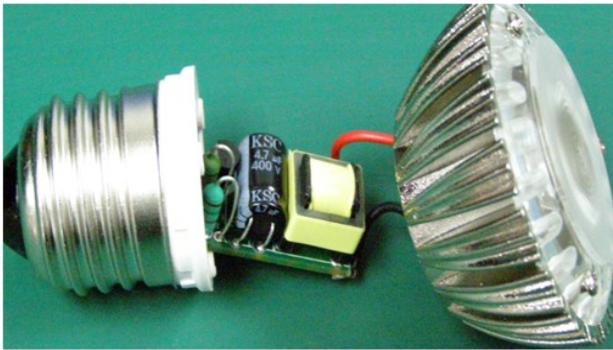
June 2014

Table of Contents

| | |
|--|----|
| ACT364 1W 350mA(3.5V) E27..... | 3 |
| ACT364 1W 350mA(3.5V) E27 Non-isolated..... | 5 |
| ACT364 3W 700mA(4V) GU10..... | 7 |
| ACT364 3W 700mA(4V) GU10 Non-isolated..... | 9 |
| ACT364 3W 350mA(12V) GU10..... | 11 |
| ACT364 3W 350mA(12V) GU10 Non-isolated..... | 13 |
| ACT365 7.8W 350mA(26V) PAR30 | 15 |
| ACT365 7.8W 350mA(26V) PAR30 Non-isolated..... | 17 |
| ACT512 16.8W 700mA(24V) PAR38 | 19 |
| ACT111A 4.8-30VDC (up to 1.5A) MR16..... | 21 |

E27 1x1W LED Lighting

| Input Voltage | Device | LED(s) | Output Voltage | Power Output | Topology |
|---------------|--------|--------|----------------|--------------|----------|
| 85 - 264VAC | ACT364 | 1 | 3.5V | 1W | Flyback |



Operation and Application

Figure 1 is the schematic of an offline LED driver using ACT364 to provide a power output of 3.5V, 350mA. This circuit is a typical flyback type power supply which includes the AC rectified circuit (BD1, C1), power drive circuit (BD pin, Q1), secondary rectified circuit (D3, C4) and the IC (ACT364) control circuit. ACT364 is a Primary Side Regulator (PSR) so that the power supply unit can regulate current and voltage without opto-coupler. Pin 4 and Pin 2 are the VDD and ground pins to provide power for the IC. Pin 3 is the base driver for the NPN transistor. Pin 1 is the switching pin. Pin 5 is the feedback pin that senses the output current and output voltage. Pin 6 is the peak current sense pin. Through a patented PSR technology, this circuit

can provide drivers for one (min), or two (max) LED lights in series due to the wide VDD operation ranges.

Key Component Selection

The turn ratio of the primary turn and the secondary turn (N_P/N_S), together with the R7 sets the maximum output current value as shown in formula (1.1). The voltage setting is through the flyback voltage of auxiliary winding and the feedback resistor R5, R6 as shown in formula (1.2). $N_P/N_S/N_{AUX}$ (160/10/23) must be designed correctly to make sure it operates in DCM mode and it can supply either one to two LEDs in same circuit. A design value V_{OUTCV} equal to 3.5V and $I_{OUTCC-MIN}$ equal to 350mA are used to do the design.

$$I_{OUTCC} = \frac{1}{2} \times L_P \times \left(\frac{0.396 \times 0.9}{R_{CS}} \right)^2 \times \left(\frac{\eta \times F_{SW}}{V_{OUTCV}} \right) \quad (1.1)$$

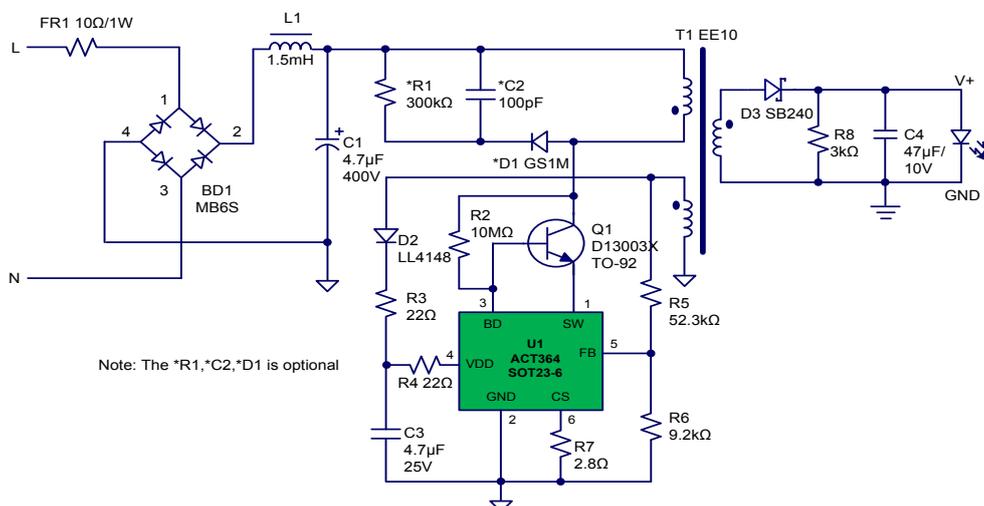
N_S and N_{AUX} are numbers of transformer secondary and auxiliary turns, and V_{SEC-R} is the rectifier diode forward drop voltage at approximately 0.1A bias.

$$V_{OUTCV} = V_{REF} \times \left(1 + \frac{R5}{R6} \right) \times \frac{N_S}{N_{AUX}} - V_{SEC-R} \quad (1.2)$$

The peak current limit is set by $(0.396 \times 0.9) / R_{CS}$.

Figure 1:

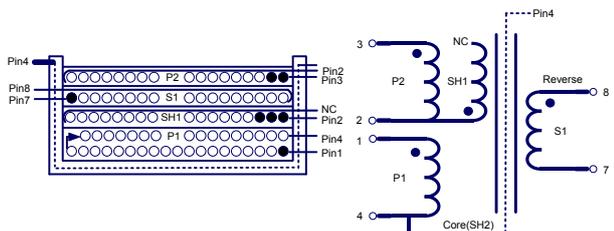
Schematic of LED Lighting Driver



Bill of Materials

| REF. | DESCRIPTION | MFTR. |
|------|---|---------|
| C1 | Capacitor, Electrolytic, 4.7µF/400V, 8×12mm | KSC |
| C2 | Capacitor, Ceramic, 100pF/500V, 1206, SMD | POE |
| C3 | Capacitor, Ceramic, 47µF/25V, 1206, SMD | POE |
| C4 | Capacitor, Ceramic, 10µF/10V, 1206, SMD | POE |
| BD1 | Bridge Rectifier, 600V/0.5A, MBS06, SDIP | PANJIT |
| D1 | Diode, U1tra Fast, GS1M, 1000V/1.0A, SMA | PANJIT |
| D2 | General Rectifier, LL4148, 100V/1A | PANJIT |
| D3 | Diode, schottky, 40V/2A, S240, SMA | PANJIT |
| L1 | Axial Inductor, 1.5mH, 0410, Dip | SoKa |
| PCB1 | PCB, L*W*T=25.5×14×1.6mm, Rev:A | Jintong |
| FR1 | Wire Round Resistor, 1W, 10ohm, KNP, 5% | TY-OHM |
| Q1 | Transistor, HFE 15-25, NPN, D13003, TO-92 | Huawai |
| R1 | Chip Resistor, 00K ohm, 0805, 5% | TY-OHM |
| R2 | Chip Resistor, 10M ohm, 1206, 5% | TY-OHM |
| R3,4 | Chip Resistor, 22 ohm, 0805, 5% | TY-OHM |
| R5 | Chip Resistor, 52.3K ohm, 0805, 1% | TY-OHM |
| R6 | Chip Resistor, 9.2K ohm, 0805, 1% | TY-OHM |
| R7 | Chip Resistor, 2.8 ohm, 1206, 5% | TY-OHM |
| R8 | Chip Resistor, 3K ohm, 0805, 5% | TY-OHM |
| T1 | Transformer, Lp=4.2mH, EE10 | |
| U1 | IC, ACT364US-T, SOT23-6 | ACT |

Transformer Specification

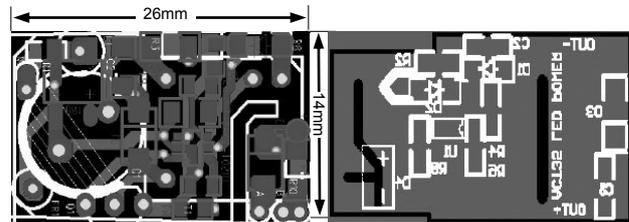


Build Up

| WINDING | TERMINAL | | TURNS | WIRE | | | INSULATION | |
|---------|----------|--------|-------|--------------|------------|-------|------------|-------|
| | START | FINISH | | TYPE | SIZE × QTY | LAYER | THICK/WIDE | LAYER |
| P1 | 1 | 4 | 160 | 2UEW | 0.1Φ×1 | 3 | 25µ/8.5mm | 2 |
| SH2 | 2 | Open | 16 | 2UEW | 0.1Φ×3 | 1 | 25µ/8.5mm | 2 |
| S1 | 8 | 7 | 10 | TEXE Reverse | 0.35Φ×1 | 1 | 25µ/8.5mm | 2 |
| P2 | 3 | 2 | 23 | 2UEW | 0.1Φ×2 | 2 | 25µ/8.5mm | 2 |
| SH2 | Core | 4 | 1 | Copper Wire | 0.18Φ×1 | 1 | 25µ/8.5mm | 2 |

Note: P1 and P2 are Primary, S1 is Secondary (Bobbin: EE-10 Horizontal).

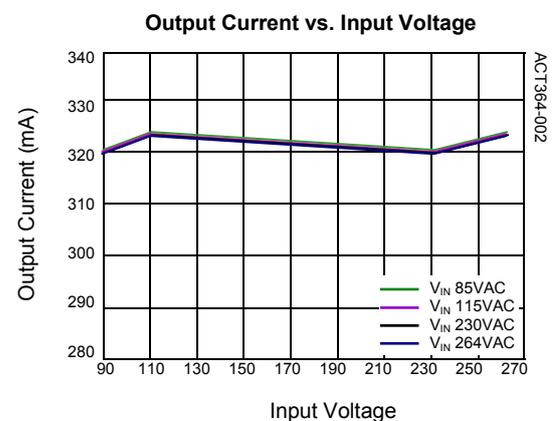
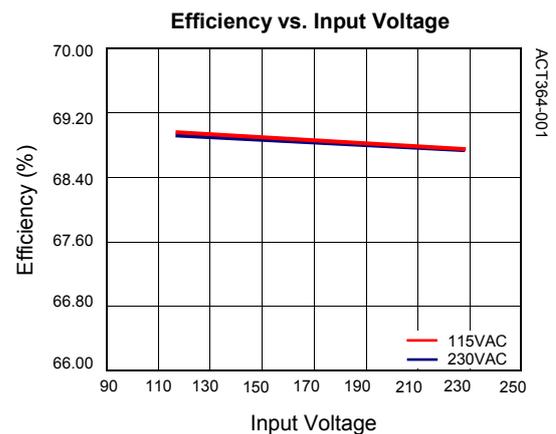
PCB Top and Bottom Layers



Electrical Specifications

| ITEM | DESCRIPTION | CONDITION | LIMITS |
|------|-----------------------|--|------------|
| 1 | Electrical Strength | 50Hz, 1 minute, from Primary and Secondary | 3kVAC |
| 2 | P1 Inductance | Inductance between pin 4 and pin 1 at 1VAC & 1kHz | 4.2mH ± 7% |
| 3 | P1 Leakage Inductance | Inductance between pin 4 and pin 1 with pins 3-2 and 8-5 shorted | 75µH |

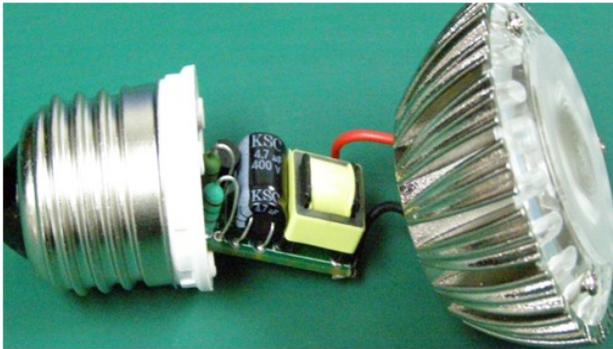
Typical performance Characteristics



| EVALUATION KITS | V _{IN} | I ₀ | LED(s) |
|-----------------|-----------------|----------------|--------|
| ACT364-LED01 | 85-264VAC | 300-350mA | 1 or 2 |

E27 1x1W LED Lighting Non-isolated

| Input Voltage | Device | LED(s) | Output Voltage | Power Output | Topology |
|---------------|--------|--------|----------------|--------------|----------|
| 85 - 264VAC | ACT364 | 1 | 3.5V | 1W | buck |



Operation and Application

Figure 1 is the schematic of an offline LED driver using ACT364 to provide a power output of 3.5V, 350mA. This circuit is tapped buck power supply which includes the AC rectified circuit (BD1, C1), power drive circuit (BD pin, Q1), secondary rectified circuit (D3, C4) and the IC (ACT364) control circuit. ACT364 is a Primary Side Regulator (PSR) so that the power supply unit can regulate current and voltage without opto-coupler. Pin 4 and Pin 2 are the VDD and ground pins to provide power for the IC. Pin 3 is the base driver for the NPN transistor. Pin 1 is the switching pin. Pin 5 is the feedback pin that senses the output current and output voltage. Pin 6 is the peak current sense pin. Through a patented PSR technology, this circuit can provide

drivers for one (min), or two (max) LED lights in series due to the wide VDD operation ranges.

Key Component Selection

The turn ratio of the primary turn and the secondary turn (N_p/N_s), together with the R7 sets the maximum output current value as shown in formula (1.1). The voltage setting is through the flyback voltage of auxiliary winding and the feedback resistor R5, R6 as shown in formula (1.2). N_p/N_{AUX} (160/23) must be designed correctly to make sure it operates in DCM mode and it can supply either one to two LEDs in same circuit. A design value V_{OUTCV} equal to 3.5V and $I_{OUTCC-MIN}$ equal to 350mA are used to do the design.

$$I_{OUTCC} = \frac{1}{2} \times L_P \times \left(\frac{0.396 \times 0.9}{R_{CS}} \right)^2 \times \left(\frac{\eta \times F_{SW}}{V_{OUTCV}} \right) \quad (1.1)$$

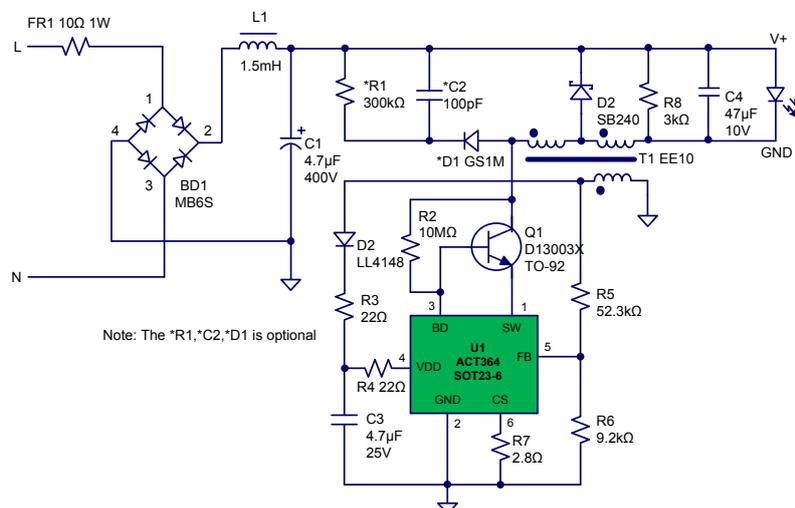
N_s and N_{AUX} are numbers of transformer secondary and auxiliary turns, and V_{SEC-R} is the rectifier diode forward drop voltage at approximately 0.1A bias.

$$V_{OUTCV} = V_{REF} \times \left(1 + \frac{R5}{R6} \right) \times \frac{N_s}{N_{AUX}} - V_{SEC-R} \quad (1.2)$$

The peak current limit is set by $(0.396 \times 0.9) / R_{CS}$.

Figure 1:

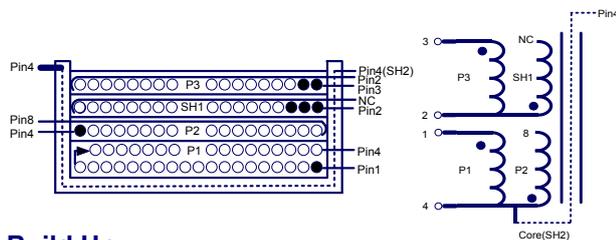
Schematic of LED Lighting Driver



Bill of Materials

| REF. | DESCRIPTION | MFTR. |
|------|---|---------|
| C1 | Capacitor, Electrolytic, 4.7µF/400V, 8×12mm | KSC |
| C2 | Capacitor, Ceramic, 100pF/500V, 1206, SMD | POE |
| C3 | Capacitor, Ceramic, 47µF/25V, 1206, SMD | POE |
| C4 | Capacitor, Ceramic, 10µF/10V, 1206, SMD | POE |
| BD1 | Bridge Rectifier, 600V/0.5A, MBS06, SDIP | PANJIT |
| D1 | Diode, U1tra Fast, GS1M, 1000V/1.0A, SMA | PANJIT |
| D2 | General Rectifier, LL4148, 100V/1A | PANJIT |
| D3 | Diode, schottky, 40V/2A, S240, SMA | PANJIT |
| L1 | Axial Inductor, 1.5mH, 0410, Dip | SoKa |
| PCB1 | PCB, L*W*T=25.5×14×1.6mm, Rev:A | Jintong |
| FR1 | Wire Round Resistor, 1W, 10ohm, KNP, 5% | TY-OHM |
| Q1 | Transistor, HFE 15-25, NPN, D13003, TO-92 | Huawai |
| R1 | Chip Resistor, 00K ohm, 0805, 5% | TY-OHM |
| R2 | Chip Resistor, 10M ohm, 1206, 5% | TY-OHM |
| R3,4 | Chip Resistor, 22 ohm, 0805, 5% | TY-OHM |
| R5 | Chip Resistor, 52.3K ohm, 0805, 1% | TY-OHM |
| R6 | Chip Resistor, 9.2K ohm, 0805, 1% | TY-OHM |
| R7 | Chip Resistor, 2.8 ohm, 1206, 5% | TY-OHM |
| R8 | Chip Resistor, 3K ohm, 0805, 5% | TY-OHM |
| T1 | Transformer, Lp=4.2mH, EE10 | |
| U1 | IC, ACT364US-T, SOT23-6 | ACT |

Transformer Specification

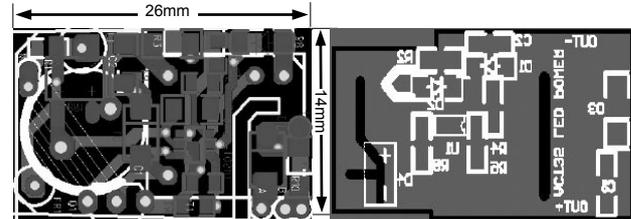


Build Up

| WINDING | TERMINAL | | TURNS | WIRE | | | INSULATION | |
|---------|----------|--------|-------|-------------|------------|-------|------------|-------|
| | START | FINISH | | TYPE | SIZE × QTY | LAYER | THICK/WIDE | LAYER |
| P1 | 1 | 4 | 150 | 2UEW | 0.1Φ×1 | 3 | 25µ/8.5mm | 2 |
| P2 | 4 | 8 | 10 | 2UEW | 0.3Φ×1 | 1 | 25µ/8.5mm | 2 |
| SH1 | 2 | NC | 16 | 2UEW | 0.1Φ×3 | 1 | 25µ/8.5mm | 2 |
| P3 | 3 | 2 | 23 | 2UEW | 0.1Φ×2 | 2 | 25µ/8.5mm | 2 |
| SH2 | Core | 4 | 1 | Copper Wire | 0.18Φ×1 | 1 | 25µ/8.5mm | 2 |

Note: P1, P2, and P3 are Primary (Bobbin: EE-10 ;Vertical).

PCB Top and Bottom Layers



Electrical Specifications

| ITEM | DESCRIPTION | CONDITION | LIMITS |
|------|--------------------------|--|------------|
| 1 | Electrical Strength | 50Hz, 1 minute, from Primary and Secondary | 3kVAC |
| 2 | P1+P2 Inductance | Inductance between pin 8 and pin 1 at 1VAC & 1kHz | 4.2mH ± 7% |
| 3 | P1+P2 Leakage Inductance | Inductance between pin 4 and pin 8 with pins 3-2 . | 75µH |

Typical performance Characteristics

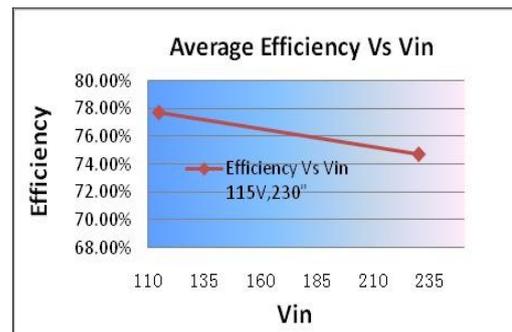


Figure 1

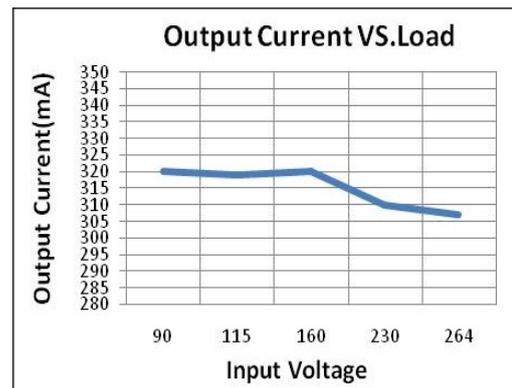


Figure 2

| EVALUATION KITS | V _{IN} | I ₀ | LED(s) |
|-----------------|-----------------|----------------|--------|
| ACT364-LED02 | 85-264VAC | 300-350mA | 1 or 2 |

GU10 1x3W LED Lighting

| Input Voltage | Device | LED(s) | Output Voltage | Power Output | Topology |
|---------------|--------|--------|----------------|--------------|----------|
| 85 - 264VAC | ACT364 | 1 | 4V | 3W | Flyback |



Operation and Application

Figure 1 is the schematic of an offline LED driver using ACT364 to provide a power output of 4V, 650mA. This circuit is a typical flyback type power supply which includes the AC rectified circuit (BD1, L1, C1), primary snubber circuit (D1, R1, C2), power drive circuit (BD pin, Q1), secondary rectified circuit (D3, C4) and the IC control circuit. ACT364 is a Primary Side Regulator (PSR) so that the power supply unit can regulate current and voltage without Opto-couple. Pin 4 and Pin 2 are the VDD and ground pins to provide power for the IC. Pin 3 is the base drive for the NPN transistor. Pin 1 is the switching pin. Pin 5 is the feedback pin that senses the output current and output voltage. Pin 6 is the peak current sense pin. Through a patented PSR

technology, this circuit can provide drivers one 3W LED lights in series due to the wide VDD operation ranges.

Key Component Selection

The turn ratio of the primary turn and the secondary turn (N_p/N_s), together with the R7 sets the maximum output current value as shown in formula (1.1). The voltage setting is through the flyback voltage of auxiliary winding and the feedback resistor R5, R6 as shown in formula (1.2). $N_p/N_s/N_{AUX}$ (160/7/22) must be designed correctly to make sure it operates in DCM mode and it can supply one LEDs in same circuit. A design value V_{OUTCV} equal to 4V and I_{OUTCC_MIN} equal to 650mA are used to do the design.

$$I_{OUTCC} = \frac{1}{2} \times L_P \times \left(\frac{0.396 \times 0.9}{R_{CS}} \right)^2 \times \left(\frac{\eta \times F_{SW}}{V_{OUTCV}} \right) \quad (1.1)$$

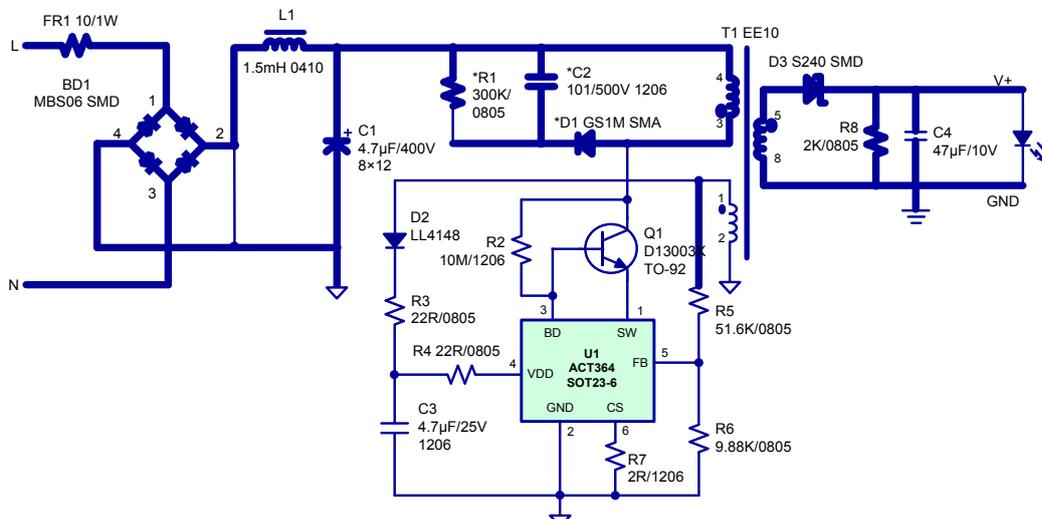
N_s and N_{AUX} are numbers of transformer secondary and auxiliary turns, and V_{SEC_R} is the rectifier diode forward drop voltage at approximately 0.1A bias.

$$V_{OUTCV} = V_{REF} \times \left(1 + \frac{R5}{R6} \right) \times \frac{N_s}{N_{AUX}} - V_{SEC_R} \quad (1.2)$$

The peak current limit is set by $(0.396 \times 0.9) / R_{CS}$.

Figure 1:

Typical Application Circuit



GU10 1x3W LED Lighting Non-isolated

| Input Voltage | Device | LED(s) | Output Voltage | Power Output | Topology |
|---------------|--------|--------|----------------|--------------|----------|
| 85 - 264VAC | ACT364 | 1 | 4V | 3W | buck |



Operation and Application

Figure 1 is the schematic of an offline LED driver using ACT364 to provide a power output of 4V, 650mA. This circuit is a tapped buck power supply which includes the AC rectified circuit (BD1, L1, C1), primary snubber circuit (D1, R1, C2), power drive circuit (BD pin, Q1), secondary rectified circuit (D3, C4) and the IC control circuit. ACT364 is a Primary Side Regulator (PSR) so that the power supply unit can regulate current and voltage without Opto-couple. Pin 4 and Pin 2 are the VDD and ground pins to provide power for the IC. Pin 3 is the base drive for the NPN transistor. Pin 1 is the switching pin. Pin 5 is the feedback pin that senses the output current and output voltage. Pin 6 is the peak current sense pin. Through a patented PSR

technology, this circuit can provide drivers one 3W LED lights in series due to the wide VDD operation ranges.

Key Component Selection

The turn ratio of the primary turn and the secondary turn (N_P/N_S), together with the R7 sets the maximum output current value as shown in formula (1.1). The voltage setting is through the flyback voltage of auxiliary winding and the feedback resistor R5, R6 as shown in formula (1.2). N_P/N_{AUX} (160/22) must be designed correctly to make sure it operates in DCM mode and it can supply one LEDs in same circuit. A design value V_{OUTCV} equal to 4V and I_{OUTCC_MIN} equal to 650mA are used to do the design.

$$I_{OUTCC} = \frac{1}{2} \times L_P \times \left(\frac{0.396 \times 0.9}{R_{CS}} \right)^2 \times \left(\frac{\eta \times F_{SW}}{V_{OUTCV}} \right) \quad (1.1)$$

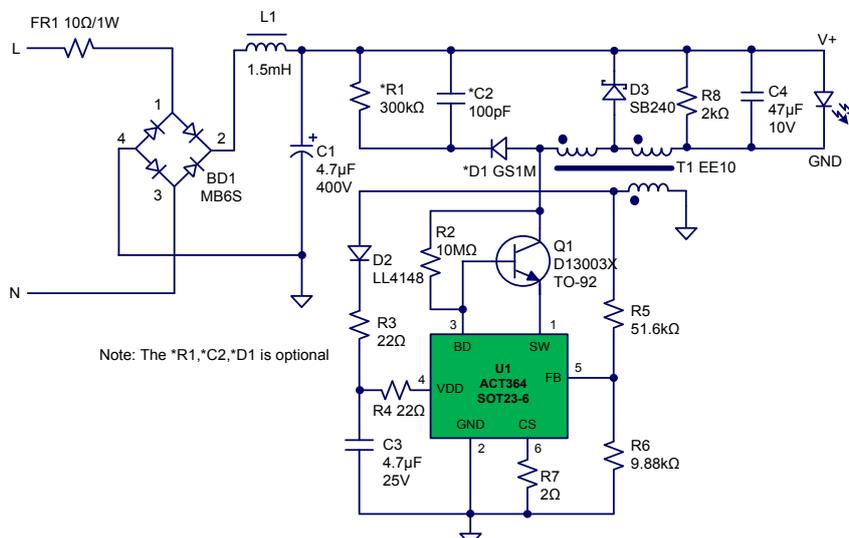
N_S and N_{AUX} are numbers of transformer secondary and auxiliary turns, and V_{SEC_R} is the rectifier diode forward drop voltage at approximately 0.1A bias.

$$V_{OUTCV} = V_{REF} \times \left(1 + \frac{R5}{R6} \right) \times \frac{N_S}{N_{AUX}} - V_{SEC_R} \quad (1.2)$$

The peak current limit is set by $(0.396 \times 0.9) / R_{CS}$.

Figure 1:

Typical Application Circuit



GU10 3x1W LED Lighting

| Input Voltage | Device | LED(s) | Output Voltage | Power Output | Topology |
|---------------|--------|--------|----------------|--------------|----------|
| 85 - 264VAC | ACT364 | 3 | 12V | 3W | Flyback |



Operation and Application

Figure 1 is the schematic of an offline LED driver using ACT364 to provide a power output of 12V, 350mA. This circuit is a typical flyback type power supply which includes the AC rectified circuit (BD1, C1, L1), primary snubber circuit (D1, R1, C2), power drive circuit (BD pin, Q1), secondary rectified circuit (D3, C4) and the IC control circuit. ACT364 is a Primary Side Regulator (PSR) so that the power supply unit can regulate current and voltage without Opto-coupler. Pin 4 and Pin 2 are the VDD and ground pins to provide power for the IC. Pin 3 is the base drive for the NPN transistor. Pin 1 is the switching pin. Pin 5 is the feedback pin that senses the output current and output voltage. Pin 6 is the

peak current sense pin. Through a patented PSR technology, this circuit can provide drivers for two (min), or three (max) LED lights in series due to the wide VDD operation ranges.

Key Component Selection

The turn ratio of the primary turn and the secondary turn (N_p/N_s), together with the R7 sets the maximum output current value as shown in formula (1.1). The voltage setting is through the flyback voltage of auxiliary winding and the feedback resistor R5, R6 as shown in formula (1.2). $N_p/N_s/N_{AUX}$ (160/20/24) must be designed correctly to make sure it operates in DCM mode and it can supply either two or three LEDs in same circuit. A design value V_{OUTCV} equal to 12V and $I_{OUTCC\ MIN}$ equal to 300mA are used to do the design.

$$I_{OUTCC} = \frac{1}{2} \times L_P \times \left(\frac{0.396 \times 0.9}{R_{CS}} \right)^2 \times \left(\frac{\eta \times F_{SW}}{V_{OUTCV}} \right) \quad (1.1)$$

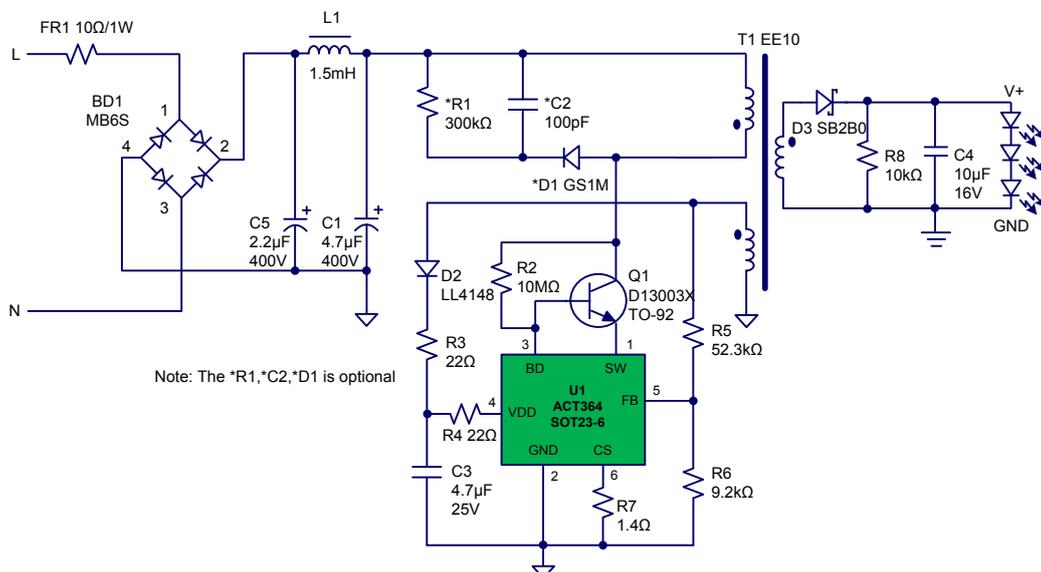
N_s and N_{AUX} are numbers of transformer secondary and auxiliary turns, and V_{SEC_R} is the rectifier diode forward drop voltage at approximately 0.1A bias.

$$V_{OUTCV} = V_{REF} \times \left(1 + \frac{R5}{R6} \right) \times \frac{N_s}{N_{AUX}} - V_{SEC_R} \quad (1.2)$$

The peak current limit is set by $(0.396 \times 0.9)/R_{CS}$.

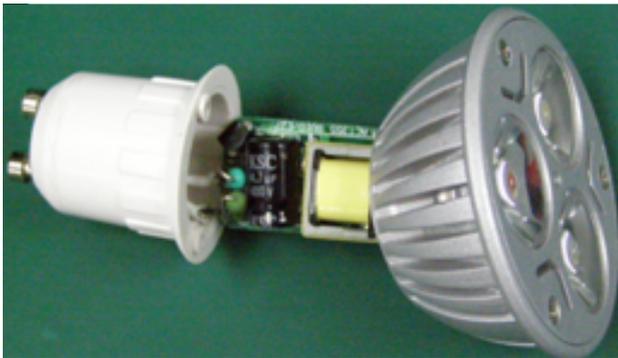
Figure 1:

Schematic of LED Lighting Driver



GU10 3x1W LED Lighting No-isolated

| Input Voltage | Device | LED(s) | Output Voltage | Power Output | Topology |
|---------------|--------|--------|----------------|--------------|----------|
| 85 - 264VAC | ACT364 | 3 | 12V | 3W | buck |



Operation and Application

Figure 1 is the schematic of an offline LED driver using ACT364 to provide a power output of 12V, 350mA. This circuit is a tapped buck power supply which includes the AC rectified circuit (BD1, C1, L1), primary snubber circuit (D1, R1, C2), power drive circuit (BD pin, Q1), secondary rectified circuit (D3, C4) and the IC control circuit. ACT364 is a Primary Side Regulator (PSR) so that the power supply unit can regulate current and voltage without Opto-coupler. Pin 4 and Pin 2 are the VDD and ground pins to provide power for the IC. Pin 3 is the base drive for the NPN transistor. Pin 1 is the switching pin. Pin 5 is the feedback pin that senses the output current and output voltage. Pin 6 is the

peak current sense pin. Through a patented PSR technology, this circuit can provide drivers for two (min), or three (max) LED lights in series due to the wide VDD operation ranges.

Key Component Selection

The turn ratio of the primary turn and the secondary turn (N_P/N_{AUX}), together with the R7 sets the maximum output current value as shown in formula (1.1). The voltage setting is through the flyback voltage of auxiliary winding and the feedback resistor R5, R6 as shown in formula (1.2). N_P/N_{AUX} (160/24) must be designed correctly to make sure it operates in DCM mode and it can supply either two or three LEDs in same circuit. A design value V_{OUT_CV} equal to 12V and $I_{OUTCC\ MIN}$ equal to 300mA are used to do the design.

$$I_{OUTCC} = \frac{1}{2} \times L_P \times \left(\frac{0.396 \times 0.9}{R_{CS}} \right)^2 \times \left(\frac{\eta \times F_{SW}}{V_{OUTCV}} \right) \quad (1.1)$$

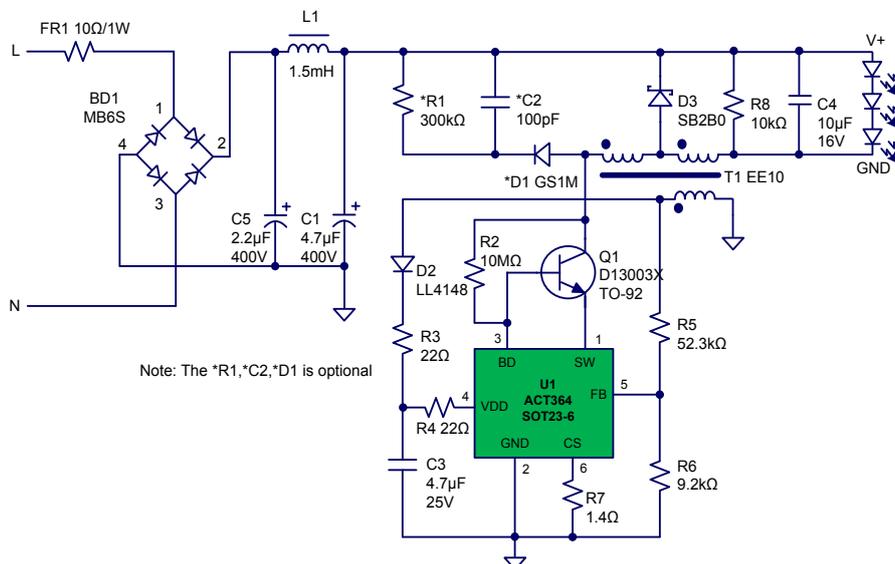
N_S and N_{AUX} are numbers of transformer secondary and auxiliary turns, and V_{SEC_R} is the rectifier diode forward drop voltage at approximately 0.1A bias.

$$V_{OUTCV} = V_{REF} \times \left(1 + \frac{R5}{R6} \right) \times \frac{N_S}{N_{AUX}} - V_{SEC_R} \quad (1.2)$$

The peak current limit is set by $(0.396 \times 0.9)/R_{CS}$.

Figure 1:

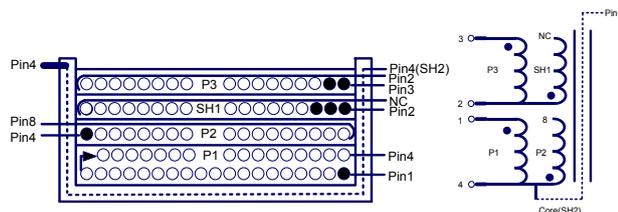
Schematic of LED Lighting Driver



Bill of Materials

| REF. | DESCRIPTION | MFTR. |
|------|---|---------|
| C1 | Capacitor, Electrolytic, 4.7µF/400V, 8×12mm | KSC |
| C2 | Capacitor, Ceramic, 100pF/500V, 1206, SMD | POE |
| C3 | Capacitor, Ceramic, 4.7µF/25V, 1206, SMD | POE |
| C4 | Capacitor, Ceramic, 10µF/16V, 1206, SMD | POE |
| C5 | Capacitor, Electrolytic, 2.2µF/400V, 6.2×12mm | KSC |
| BD1 | Bridge Rectifier, 600V/0.5A, MBS06, SDIP | PANJIT |
| D1 | Diode, Ultra Fast, GS1M, 1000V/1.0A, SMA | PANJIT |
| D2 | General Rectifier, LL4148, 100V/1A | PANJIT |
| D3 | Diode, Schottky, 200V/1A, SB2B0, SMA | PANJIT |
| L1 | Axial Inductor, 1.5mH, 0410, Dip | SoKa |
| PCB1 | PCB, L*W*T=25.5×14×1.6mm, Rev:A | Jintong |
| FR1 | Wire Round Resistor, 1W, 10ohm, KNP, 5% | TY-OHM |
| Q1 | Transistor, HFE15-25, NPN, D13003, TO-92 | Huawai |
| R1 | Chip Resistor, 300K ohm, 0805, 5% | TY-OHM |
| R2 | Chip Resistor, 10M ohm, 1206, 5% | TY-OHM |
| R3,4 | Chip Resistor, 22 ohm, 0805, 5% | TY-OHM |
| R5 | Chip Resistor, 52.3K ohm, 0805, 1% | TY-OHM |
| R6 | Chip Resistor, 9.2K ohm, 0805, 1% | TY-OHM |
| R7 | Chip Resistor, 1.4 ohm, 1206, 5% | TY-OHM |
| R8 | Chip Resistor, 10K ohm, 0805, 5% | TY-OHM |
| T1 | Transformer, Lp=2.1mH, EE10 | |
| U1 | IC, ACT364US-T, SOT23-6 | ACT |

Transformer Specification

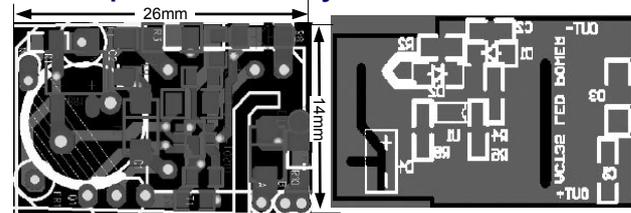


Build Up

| WINDING | TERMINAL | | TURNS | WIRE | | | INSULATION | |
|---------|----------|--------|-------|-------------|------------|-------|------------|-------|
| | START | FINISH | | TYPE | SIZE × QTY | LAYER | THICK/WIDE | LAYER |
| P1 | 1 | 4 | 140 | 2UEW | 0.1Φ×1 | 3 | 25µ/8.5mm | 2 |
| P2 | 4 | 8 | 20 | 2UEW | 0.3Φ×1 | 1 | 25µ/8.5mm | 2 |
| SH1 | 2 | NC | 16 | 2UEW | 0.1Φ×3 | 1 | 25µ/8.5mm | 2 |
| P3 | 3 | 2 | 24 | 2UEW | 0.1Φ×2 | 2 | 25µ/8.5mm | 2 |
| SH2 | Core | 4 | 1 | Copper Wire | 0.18Φ×1 | 1 | 25µ/8.5mm | 2 |

Note: P1 and P2 and P3 are Primary (Bobbin: EE-10 ; Vertical).

PCB Top and Bottom Layers



Electrical Specifications

| ITEM | DESCRIPTION | CONDITION | LIMITS |
|------|--------------------------|--|------------|
| 1 | Electrical Strength | 50Hz, 1 minute, from Primary and Secondary | 3kVAC |
| 2 | P1+P2 Inductance | Inductance between pin 1 and pin 8 at 1VAC & 1kHz | 2.1mH ± 7% |
| 3 | P1+P2 Leakage Inductance | Inductance between pin 1 and pin 8 with pins 2-3 shorted | 75µH |

Typical Performance Characteristics

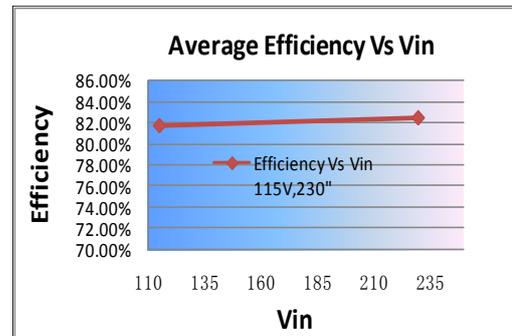


Figure 1

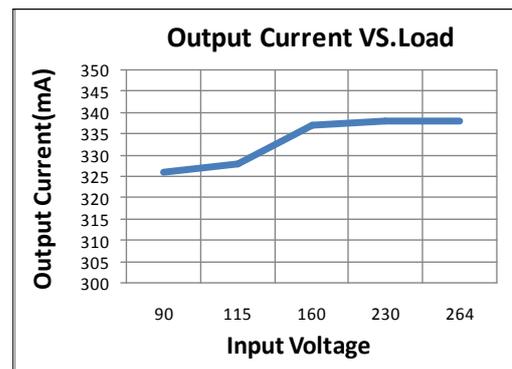


Figure 2

| EVALUATION KITS | V _{IN} | I _O | LED(s) |
|-----------------|-----------------|----------------|--------|
| ACT364-LED06 | 85-264VAC | 280-350mA | 2 or 3 |

PAR30 7x1W LED Lighting

| Input Voltage | Device | LED(s) | Output Voltage | Power Output | Transformer | Topology |
|---------------|--------|--------|----------------|--------------|-------------|----------|
| 85 - 264VAC | ACT365 | 7 | 26V | 7.8W | EE16 | Flyback |



Operation and Application

Figure 1 is the schematic of LED lighting using ACT365 to provide output power of 26V/300mA with PF>0.77. This circuit is a typical flyback power supply which includes the AC rectified circuit (BD1, C2, C3), power drive circuit (BD pin, Q1), power factor rectified circuit (D1-D3, C2, C3), secondary rectified circuit (D6, C7, C8) and the IC control circuit. ACT365 is a Primary Side Regulator (PSR) so that the power supply unit can regulate current and voltage without Opto-coupler. Pin 4 and Pin 2 are the VDD and ground pins to provide power for the IC. Pin 3 is the base drive for the NPN transistor. Pin 1 is the switching pin. Pin 5 is the feedback pin that senses the output current and output voltage. Pin 6 is the peak current sense pin. Resistance of R10 determines the output DC cord compensation percentage.

Through a patented PSR technology, this circuit can provide drivers for five (min), or seven (max) LED lights in series due to the wide VDD operation ranges.

Key Component Selection

The maximum output current is decided by formula (1).

$$I_{OUTCC} = \frac{1}{2} \times L_P \times \left(\frac{0.9 \times 0.396}{R_{CS}} \right)^2 \times \left(\frac{\eta \times F_{SW}}{V_{OUTCC}} \right) \quad (1)$$

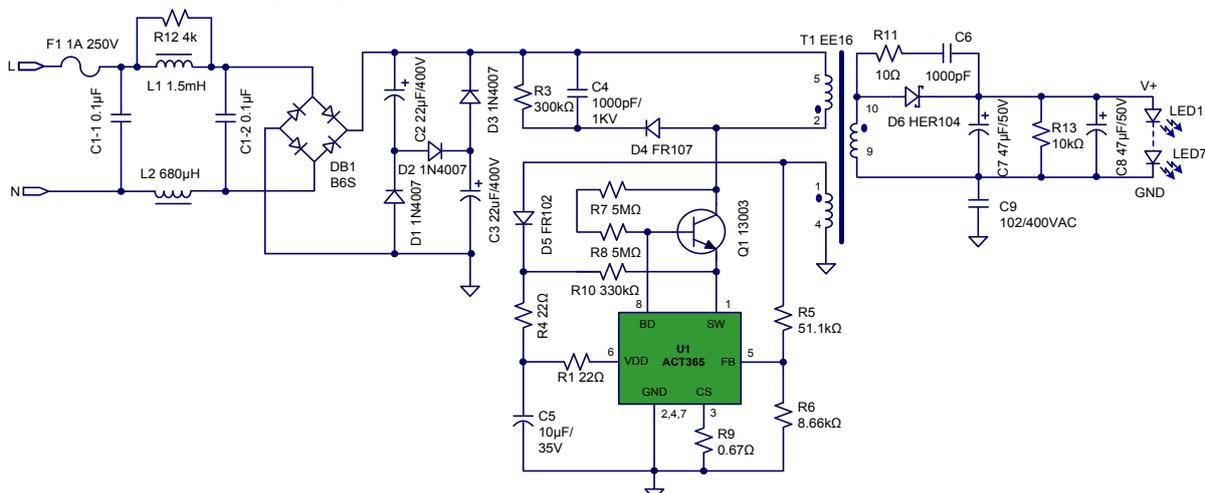
Lp is the transformer inductance value, Rcs is the current sense resistor, which is shown as R9 in the schematic. Fsw is the switching frequency, which design value is 75kHz. η is the overall system efficiency, which value is approximately equal to 75%. Voutcc is the output voltage, which setting is through the flyback voltage of auxiliary winding and the feedback resistor R5, R6 as shown in formula (2).

$$V_{OUTCC} = V_{REF} \times \left(1 + \frac{R_5}{R_6} \right) \times \frac{N_S}{N_{AUX}} - V_{SEC_R} \quad (2)$$

Np/Ns/Naux (102/23/13) must be designed correctly to ensure it operates in DCM in all conditions. A design value Voutcc equal to 26V and Ioutcc_min equal to 300mA are used to do the design. Ns and Naux are number of turns of secondary and auxiliary of the transformer. VSEC_R is the forward voltage drop of the output rectifier diode at approximately 0.1A bias. The peak current limit is set by (0.396×0.9)/Rcs.

Figure 1:

Schematic of LED Lighting Driver



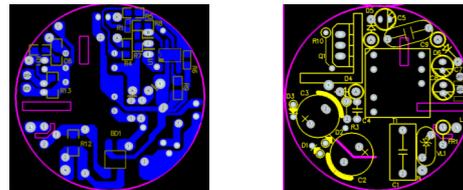
Bill of Materials

| REF | DESCRIPTION | MFTR |
|--------|---|----------|
| C1-1/2 | X1 Capacitor,0.1μF/400V,13x6x11mm | USE |
| C2,C3 | Capacitor,Electrolytic, 22μF/250V, 10x14mm | KSC |
| C4 | Capacitor,Ceramic,1000pF/1KV, DIP | POE |
| C5 | Capacitor,Electrolytic,10μF/35V, 5x11mm | KSC |
| C6 | Capacitor,Ceramic,1000pF/50V,1206 | POE |
| C7,C8 | Capacitor,Electrolytic, 47μF/50V, 6.3x12mm | KSC |
| C9 | Y cap,1000pF/275V,Dip | USE |
| BD1 | Bridge,B6S,600V/0.5A,MDI,SMD | PANJIT |
| D1~D3 | Fast Recovery Rectifiers,1N4007, DO-41 | Good-Ark |
| D4 | Fast Recovery Rectifier ,FR107,DO-41 | Good-Ark |
| D5 | Fast Recovery Rectifier ,FR102,DO-41 | Good-Ark |
| D6 | Efficiency Rectifiers, 300V/1A ,HER104, DO-41 | Good-Ark |
| L1 | Axial Inductor,1.5mH, φ5x7mm,Dip | SoKa |
| L2 | I-shaped Inductor,680μH,0410,Dip | SoKa |
| Q1 | Transistor, HFE 20-25 NPN, D13003, TO-126 | Huawei |
| PCB1 | PCB, ACT365_LED_01,Rev:A | Jintong |
| F1 | Fuse:3.15A 250V 3.6*10mm With Pigtail | walter |
| R1,R4 | Chip Resistor, 22Ω, 0805, 5% | TY-OHM |
| R3 | Chip Resistor, 300kΩ, 1W, 5% | TY-OHM |
| R5 | Chip Resistor, 51.1kΩ, 0805,1% | TY-OHM |
| R6 | Chip Resistor, 8.66kΩ, 0805, 1% | TY-OHM |
| R7,R8 | Chip Resistor, 5MΩ, 0805, 5% | TY-OHM |
| R9 | Chip Resistor, 0.67Ω, 1206,1% | TY-OHM |
| R10 | Chip Resistor, 330kΩ, 1/4W, 5% | TY-OHM |
| R11 | Chip Resistor, 10Ω, 0805, 5% | TY-OHM |
| R12 | Chip Resistor, 4.0kΩ, 0805, 5% | TY-OHM |
| R13 | Chip Resistor, 10kΩ, 0805, 5% | TY-OHM |
| T1 | Transformer, Lp=1.0mH, EE16, Vertical | |
| U1 | IC, ACT365SH-T ,SOP-8 | |

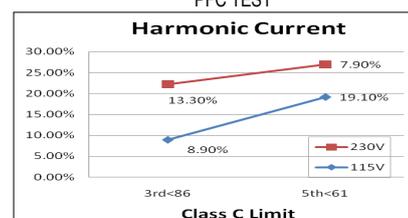
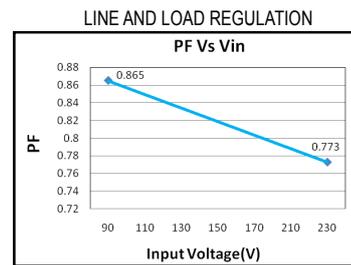
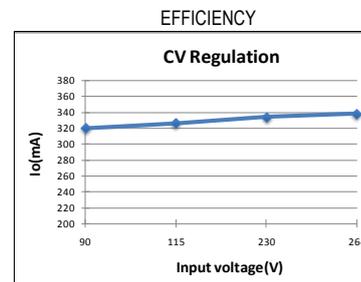
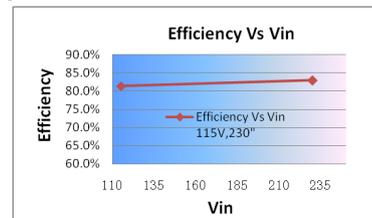
Electrical Specifications

| ITEM | DESCRIPTION | CONDITION | LIMITS |
|------|-----------------------|--|------------|
| 1 | Electrical Strength | 50Hz, 1 minute, from Primary and Secondary | 3kVAC |
| 2 | P1 Inductance | Inductance between pin 2 and pin 5 at 1VAC & 1kHz | 1.0mH ± 7% |
| 3 | P1 Leakage Inductance | Inductance between pins 2 and pin 5 with pins 4-1 and 8-10 shorted | 75μH |

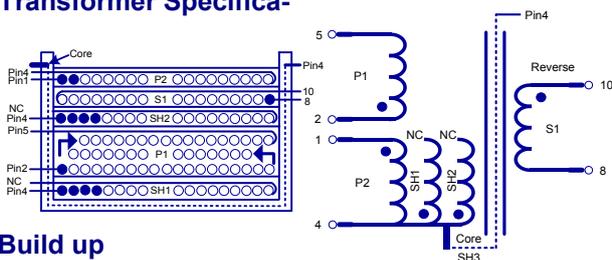
PCB Layout



Typical performance Characteristics



Transformer Specifica-



Build up

| WINDING | TERMINAL | | TURNS | WIRE | | | INSULATION | |
|---------|----------|--------|-------|--------------|------------|-------|------------|-------|
| | START | FINISH | | TYPE | SIZE × QTY | LAYER | THICK/WIDE | LAYER |
| SH1 | 4 | NC | 14 | 2UEW | 0.12Φ*4 | 1 | 0.025*8.5W | 2 |
| P1 | 2 | 5 | 102 | 2UEW | 0.23Φ*1 | 3 | 0.025*8.5W | 2 |
| SH2 | 4 | NC | 14 | 2UEW Reverse | 0.12Φ*4 | 1 | 0.025*8.5W | 2 |
| S1 | 8 | 10 | 23 | TEX-E | 0.35Φ*1 | 1 | 0.025*8.5W | 2 |
| P2 | 1 | 4 | 13 | 2UEW | 0.12Φ*2 | 1 | 0.025*8.5W | 2 |
| SH3 | core | 4 | 3 | conductor | 0.15Φ*1 | 1 | 0.025*10 | 8 |

Note: SH1,SH2,and SH3 are shielding; P1 and P2 are Primary, S1 is Secondary (Bobbin: EE-16, Vertical).

| EVALUATION KITS | V _{IN} | V _O | I _O |
|-----------------|-----------------|----------------|----------------|
| ACT365-LED01 | 85-264VAC | 26V | 300-400mA |

PAR30 7x1W LED Lighting Non-isolated

| Input Voltage | Device | LED(s) | Output Voltage | Power Output | Transformer | Topology |
|---------------|--------|--------|----------------|--------------|-------------|----------|
| 85 - 264VAC | ACT365 | 7 | 26V | 7.8W | EE16 | Flyback |



Operation and Application

Figure 1 is the schematic of LED lighting using ACT365 to provide output power of 26V300mA with PF>0.77. This circuit is a typical flyback power supply which includes the AC rectified circuit (BD1, C2, C3), power drive circuit (BD pin, Q1), power factor rectified circuit (D1-D3, C2, C3), secondary rectified circuit (D6, C7, C8) and the IC control circuit. ACT365 is a Primary Side Regulator (PSR) so that the power supply unit can regulate current and voltage without Opto-coupler. Pin 4 and Pin 2 are the VDD and ground pins to provide power for the IC. Pin 3 is the base drive for the NPN transistor. Pin 1 is the switching pin. Pin 5 is the feedback pin that senses the output current and output voltage. Pin 6 is the peak current sense pin. Resistance of R10 determines the output DC cord compensation percentage.

Through a patented PSR technology, this circuit can provide drivers for five (min), or seven (max) LED lights in series due to the wide VDD operation ranges.

Key Component Selection

The maximum output current is decided by formula (1).

$$I_{OUTCC} = \frac{1}{2} \times L_P \times \left(\frac{0.9 \times 0.396}{R_{CS}} \right)^2 \times \left(\frac{\eta \times F_{SW}}{V_{OUTCC}} \right) \quad (1)$$

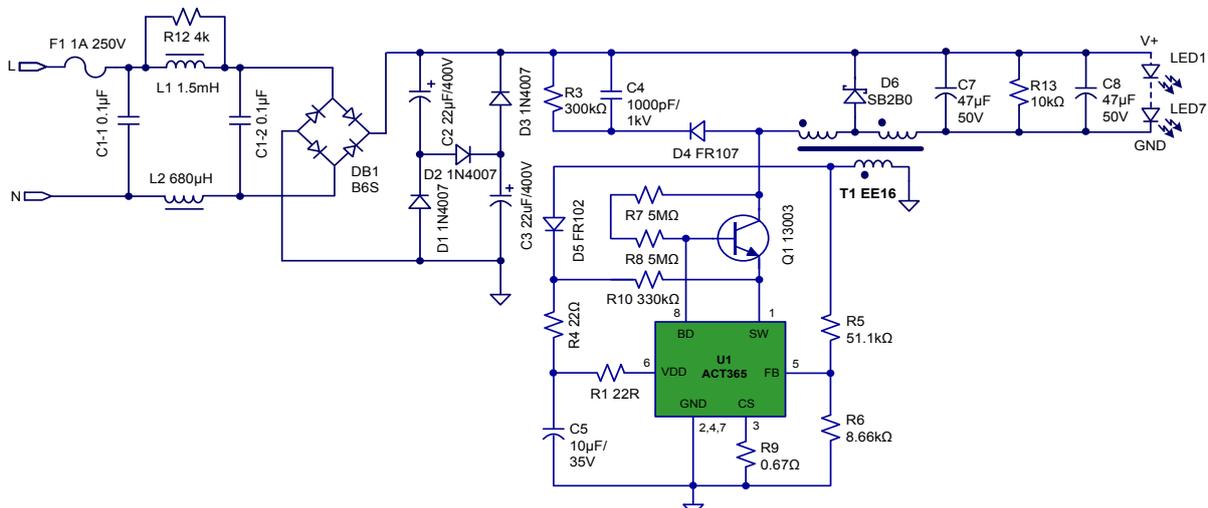
L_P is the transformer inductance value, R_{CS} is the current sense resistor, which is shown as R9 in the schematic. F_{SW} is the switching frequency, which design value is 75kHz. η is the overall system efficiency, which value is approximately equal to 75%. V_{outcc} is the output voltage, which setting is through the flyback voltage of auxiliary winding and the feedback resistor R5, R6 as shown in formula (2).

$$V_{OUTCC} = V_{REF} \times \left(1 + \frac{R_5}{R_6} \right) \times \frac{N_S}{N_{AUX}} - V_{SEC_R} \quad (2)$$

$N_P/N_S/N_{AUX}$ (102/23/13) must be designed correctly to ensure it operates in DCM in all conditions. A design value V_{outcc} equal to 26V and I_{outcc_min} equal to 300mA are used to do the design. N_S and N_{AUX} are number of turns of secondary and auxiliary of the transformer. V_{SEC_R} is the forward voltage drop of the output rectifier diode at approximately 0.1A bias. The peak current limit is set by $(0.396 \times 0.9)/R_{CS}$.

Figure 1:

Schematic of LED Lighting Driver



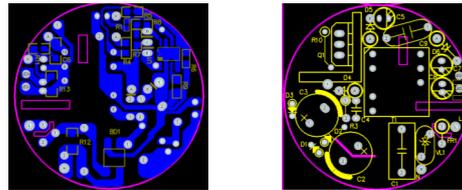
Bill of Materials

| REF | DESCRIPTION | MFTR |
|--------|---|----------|
| C1-1/2 | X1 Capacitor,0.1μF/400V,13x6x11mm | USE |
| C2,C3 | Capacitor,Electrolytic, 22μF/250V, 10x14mm | KSC |
| C4 | Capacitor,Ceramic,1000pF/1KV, DIP | POE |
| C5 | Capacitor,Electrolytic,10μF/35V, 5x11mm | KSC |
| C6 | Capacitor,Ceramic,1000pF/50V,1206 | POE |
| C7,C8 | Capacitor,Electrolytic, 47μF/50V, 6.3x12mm | KSC |
| C9 | Y cap,1000pF/275V,Dip | USE |
| BD1 | Bridge,B6S,600V/0.5A,MDI,SMD | PANJIT |
| D1~D3 | Fast Recovery Rectifiers,1N4007, DO-41 | Good-Ark |
| D4 | Fast Recovery Rectifier ,FR107,DO-41 | Good-Ark |
| D5 | Fast Recovery Rectifier ,FR102,DO-41 | Good-Ark |
| D6 | Efficiency Rectifiers, 300V/1A ,HER104, DO-41 | Good-Ark |
| L1 | Axial Inductor,1.5mH, φ5x7mm,Dip | SoKa |
| L2 | I-shaped Inductor.680μH,0410,Dip | SoKa |
| Q1 | Transistor, HFE 20-25 NPN, D13003, TO-126 | Huawei |
| PCB1 | PCB, ACT365_LED_01,Rev:A | Jintong |
| F1 | Fuse:3.15A 250V 3.6*10mm With Pigtail | walter |
| R1,R4 | Chip Resistor, 22Ω, 0805, 5% | TY-OHM |
| R3 | Chip Resistor, 300kΩ, 1W, 5% | TY-OHM |
| R5 | Chip Resistor, 51.1kΩ, 0805,1% | TY-OHM |
| R6 | Chip Resistor, 8.66kΩ, 0805, 1% | TY-OHM |
| R7,R8 | Chip Resistor, 5MΩ, 0805 , 5% | TY-OHM |
| R9 | Chip Resistor, 0.67Ω, 1206,1% | TY-OHM |
| R10 | Chip Resistor, 330kΩ, 1/4W, 5% | TY-OHM |
| R11 | Chip Resistor, 10Ω, 0805, 5% | TY-OHM |
| R12 | Chip Resistor, 4.0kΩ, 0805, 5% | TY-OHM |
| R13 | Chip Resistor, 10kΩ, 0805, 5% | TY-OHM |
| T1 | Transformer, Lp=1.0mH, EE16, Vertical | |
| U1 | IC, ACT365SH-T ,SOP-8 | |

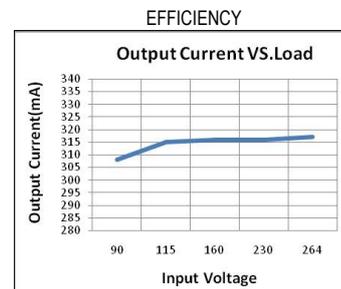
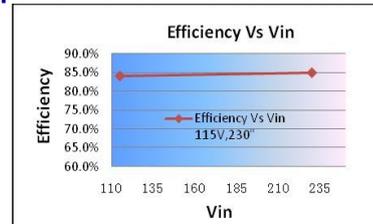
Electrical Specifications

| ITEM | DESCRIPTION | CONDITION | LIMITS |
|------|--------------------------|--|------------|
| 1 | Electrical Strength | 50Hz, 1 minute, from Primary and Secondary | 3kVAC |
| 2 | P1+P2 Inductance | Inductance between pin 2 and pin 8 at 1VAC & 1kHz | 2.0mH ± 7% |
| 3 | P1+P2 Leakage Inductance | Inductance between pins 2 and pin8 with pins 4-1 shorted | 75μH |

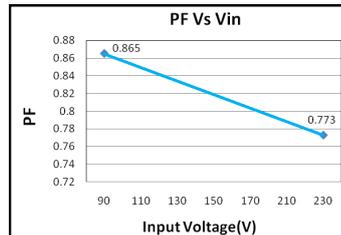
PCB Layout



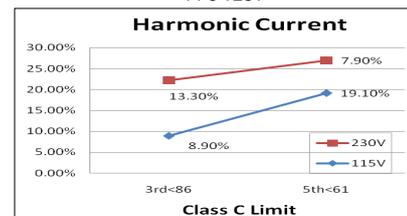
Typical performance Characteristics



LINE AND LOAD REGULATION



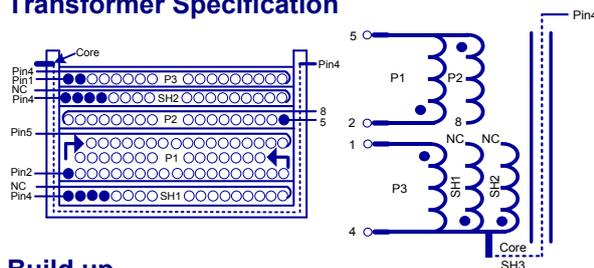
PFC TEST



HARMONIC CURRENT

| EVALUATION KITS | V _{IN} | V _O | I _O |
|-----------------|-----------------|----------------|----------------|
| ACT365-LED02 | 85-264VAC | 26V | 300-400mA |

Transformer Specification



Build up

| WINDING | TERMINAL | | TURNS | WIRE | | | INSULATION | |
|---------|----------|--------|-------|-----------|------------|-------|------------|-------|
| | START | FINISH | | TYPE | SIZE × QTY | LAYER | THICK/WIDE | LAYER |
| SH1 | 4 | NC | 14 | 2UEW | 0.12Φ*4 | 1 | 0.025*8.5W | 2 |
| P1 | 2 | 5 | 80 | 2UEW | 0.2Φ*1 | 2 | 0.025*8.5W | 2 |
| P2 | 5 | 8 | 23 | 2UEW | 0.35Φ*1 | 1 | 0.025*8.5W | 2 |
| SH2 | 4 | NC | 14 | 2UEW | 0.12Φ*4 | 1 | 0.025*8.5W | 2 |
| S1 | 8 | 10 | 23 | 2UEW | 0.35Φ*1 | 1 | 0.025*8.5W | 2 |
| P3 | 1 | 4 | 13 | 2UEW | 0.12Φ*2 | 1 | 0.025*8.5W | 2 |
| SH3 | core | 4 | 3 | conductor | 0.15Φ*1 | 1 | 0.025*10 | 8 |

Note: SH1,SH2,and SH3 are shielding; P1,P2 and P3 are Primary, (Bobbin: EE-16, Vertical).

PAR38 7x3W LED Lighting

| Input Voltage | Device | LED(s) | Output Voltage | Power Output | Transformer | Topology |
|---------------|--------|--------|----------------|--------------|-------------|----------|
| 85 - 264VAC | ACT512 | 7 | 24V | 16.8W | EF20 | Flyback |



Key Component Selection

The maximum output current is decided by formula (1).

$$I_{outcc} = 2.5 \times \frac{R16}{R15 \times (R12 // R13)} \quad (1)$$

Its output voltage or number of LED is roughly decided by formula (2).

$$V_{outlv} = \left(2.5 \times \frac{R21 + R20}{R20} \right) + \left(\frac{R21}{R20} * I_o * (R12 // R13) \right) \quad (2)$$

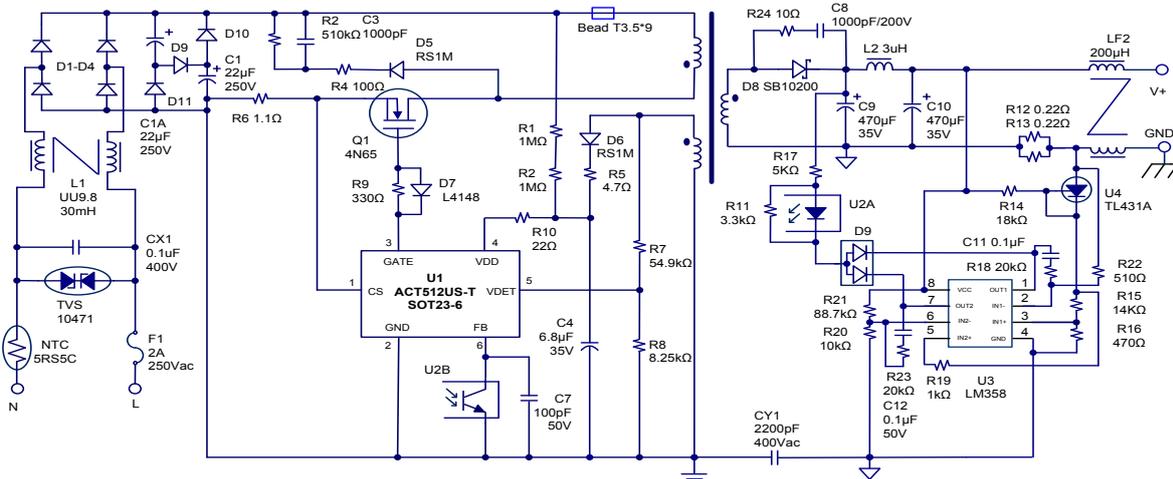
Operation and Application

Figure 1 is the schematic of LED lighting using ACT512 to provide output power of 24V700mA with PF>0.9. This circuit is a typical flyback power supply which includes the AC rectified circuit (D1-D4, C1A, C1), power drive circuit (GATE pin, Q1), power factor rectified circuit (D9-D11, C1A, C1), secondary rectified circuit (D8, C9, C10) and the IC control circuit. ACT512 is a CCM & Quasi-Resonant PWM Controller. Pin 4 and Pin 2 are the VDD and ground pins to provide power for the IC. Pin 3 is the gate drive pin for the MOSFET. Pin 1 is the Current Sense Pin. Pin 5 is the Valley Detector Pin. Pin 6 is the Feedback Pin.

The transformer design procedure can refer to the design example section of ACT512 DS. In this design, Np/Ns/Naux is set as 80/36/25 to ensure it operates in CCM to improve efficiency. Independent Output Short Protection, OTP, OVP, Brown Out Protection, Rcs Short/Open Protection, Transformer Winding Short Protection, Output Diode Short/Open Protection, Open Loop Protection, are integrated to protect damage on circuits and LED die itself.

This circuit can provide drivers for five (min), or seven (max) LED lights in series due to the wide VDD operation ranges. Accurate current control is through R12/R13 and LM358 control circuit.

Figure 1:
Schematic of LED Lighting Driver



Bill of Materials

| REF | DESCRIPTION | MFTR |
|--------------|---|-------------|
| IC1 | IC, ACT512, SOT23-6 | Active-Semi |
| C1A | Capacitor, Electrolytic, 22µF/250V, 10 × 16mm | KSC |
| C1 | Capacitor, Electrolytic, 22µF/250V, 10 × 16mm | KSC |
| C3 | Capacitor, Ceramic, 1000pF/0.5KV,SMD | POE |
| C4 | Capacitor, Electrolytic, 6.8µF/35V, 5*11mm | KSC |
| C7 | Capacitor, Ceramic, 1000PF/50V,0805,SMD | POE |
| C8 | Capacitor, Ceramic, 1000PF/100V,0805,SMD | POE |
| C9,C10 | Capacitor, Electrolytic, 470µF/35V, 8*16mm | POE |
| C11,C12 | Capacitor, Ceramic, 0.1µF/50V,0805,SMD | POE |
| D1-D4,D9-D11 | Diode, 1N4007,1A1000V DO-41 | Good-Ark |
| D5,D6 | RS1M SMD | Good-Ark |
| D7 | Diode L4148 SMD | Good-Ark |
| D8 | Diode, Schottky, 200V/10A, SBR10200, DO-220 | Good-Ark |
| LF1 | CM Inductor, 20mH, UU9.8 | SoKa |
| LF2 | Axial Inductor, 0.55*5T, 5*7,Dip 200uH | SoKa |
| L2 | DM Inductor, 3µH, R5 | SoKa |
| Q1 | Mosfet Transistor, 04N65, TO-220 | ST |
| PCB1 | PCB, L*W*T =49x68x1.6mm, Cem-1, Rev.A | Jintong |
| F1 | Fusible, 2A/250V | TY-OHM |
| R1,R2 | Chip Resistor,1M, SMD 0805, 5% | TY-OHM |
| R3 | metal Resistor,400K Ω, 1206,5% | TY-OHM |
| R4 | Chip Resistor, 100Ω, 0805, 5% | TY-OHM |
| R5 | Chip Resistor,4.7K, 0805, 5% | TY-OHM |
| R6 | Chip Resistor,1Ω, 1206, 1% | TY-OHM |
| R7 | Chip Resistor, 78KΩ, 0805, 1% | TY-OHM |
| R8 | Chip Resistor, 11.7KΩ, 0805, 1% | TY-OHM |
| R9 | Chip Resistor, 330Ω, 0805, 5% | TY-OHM |
| R10 | Chip Resistor, 22Ω, 0805, 5% | TY-OHM |
| R11 | Chip Resistor, 6KΩ, 0805, 5% | TY-OHM |
| R12,R13 | Chip Resistor, 0.22Ω, 1206, 5% | TY-OHM |
| R14 | Chip Resistor, 18KΩ, 0805, 5% | TY-OHM |
| R15 | Chip Resistor,14KΩ, 0805,5% | TY-OHM |
| R16 | Chip Resistor,510Ω, 0805,1% | TY-OHM |
| R17 | Chip Resistor,5KΩ, 0805, 5% | TY-OHM |
| R18,R23 | Chip Resistor,20KΩ, 0805, 5% | TY-OHM |
| R19 | Chip Resistor,1KΩ, 0805, 5% | TY-OHM |
| R20 | Chip Resistor,10KΩ, 0805,1% | TY-OHM |
| R21 | Chip Resistor,86KΩ, 0805,1% | TY-OHM |
| R22 | Chip Resistor,510Ω, 0805,5% | TY-OHM |
| R24 | Chip Resistor,22Ω, 1206,5% | TY-OHM |
| T1 | EF20 | ACT |
| CX1 | X capacitance, 0.1µF/400V,X1 | |
| NTC | Thermistor, SC053 | |
| TVS | Varistor, 7D471 | |
| CY1 | Y capacitance, 1000pF/400V,Y1 | SEC |
| IC2 | Opto-coupler, PC817C CTR=200 dip-4 | Sharp |
| IC3 | IC LM358 SOP-8 | ST |
| IC4 | Voltage Regulator, TL431A, Vref=2.5V TO-92 | ST |

Transformer Specification



Build up

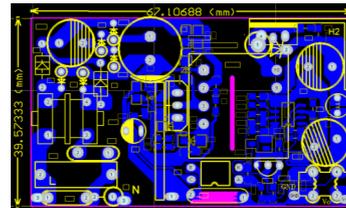
| WINDING | TERMINAL | | | WIRE | | | INSULATION | |
|---------|----------|--------|-------|-----------|------------|-------|------------|-------|
| | START | FINISH | TURNS | TYPE | SIZE × QTY | LAYER | THICK/WIDE | LAYER |
| P1 | 3 | 5 | 40 | 2UEW | 0.28Φ*1 | 1 | 0.025*11W | 2 |
| SH1 | NC | 1 | 0.9 | copper | 10mm | 1 | 0.025*11W | |
| S1 | 9 | 10 | 36 | TEX-E | 0.4Φ*1 | 2 | 0.025*11W | 2 |
| P2 | 4 | 1 | 25 | 2UEW | 0.15Φ*2 | 1 | 0.025*11W | 2 |
| P3 | 5 | 2 | 40 | 2UEW | 0.28Φ*1 | 1 | 0.025*11W | 2 |
| SH2 | core | 1 | 3 | conductor | 0.15Φ*1 | 1 | 0.025*10 | 8 |

Note: SH1,SH2are shielding; P1,P2 and P3 are Primary, (Bobbin: EF-20, level).

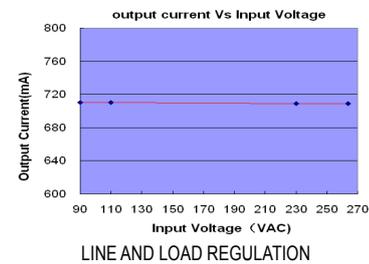
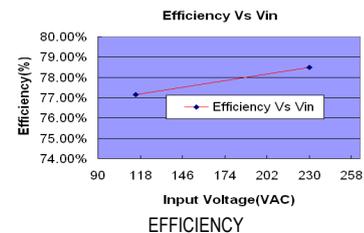
Electrical Specifications

| ITEM | DESCRIPTION | CONDITION | LIMITS |
|------|-----------------------|--|-------------|
| 1 | Electrical Strength | 50Hz, 1 minute, from Primary and Secondary | 3kVAC |
| 2 | P1 Inductance | Inductance between pin 2 and pin 3 at 1VAC & 1kHz | 0.82mH ± 7% |
| 3 | P1 Leakage Inductance | Inductance between pins 2 and pin3 with pins 4-1 shorted | 75µH |

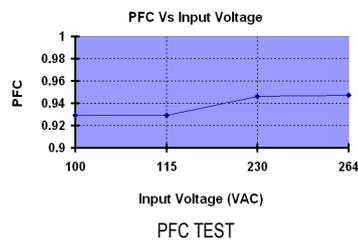
PCB Layout



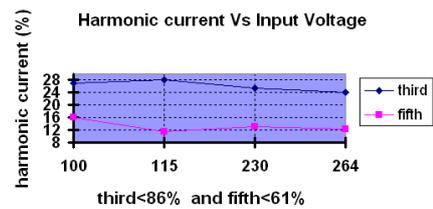
Typical performance Characteristics



LINE AND LOAD REGULATION



PFC TEST



third<86% and fifth<61%

HARMONIC CURRENT

| EVALUATION KITS | V _{IN} | V _O | I _O |
|-----------------|-----------------|----------------|----------------|
| ACT512-LED01 | 85-264VAC | 24V | 700-720mA |

ACT111A High Efficiency, Low Cost HB LED Lighting

| Input Voltage | LED # | Output Current | V _{FB} | Topology |
|---------------|-------|----------------|-----------------|----------|
| 4.8 – 30VDC | 1-6 | 1.5A | 100mV | Buck |

Circuit Bottom View
Circuit Top View


Design Features

- ◆ 95% Efficiency
- ◆ 4.8V to 30V Input and up to 1.5A Output
- ◆ 1.4 MHz Switching & Small SOT23-6 Package
- ◆ PWM (0-100%, 0.1-10kHz) Dimming
- ◆ **Thermal Shutdown & Short Circuit Protection**

Operation and Application

The bridge rectifier is for AC input only. The DC input is directly connected to IN and ground. The ACT111A has an under-voltage lockout (UVLO) at 4.0V with 250mV hysteresis. When input voltage falls below 4.0V, SW stops switching. The device is activated as input voltage goes higher than 4.2V.

The LED output current is sensed by a resistor in series with the LED. The ACT111A precisely regulates the LED current by the internal EA and 0.1V reference. The average LED current is determined by the equation: $I_{LED} = \frac{0.1V}{R_{SENSE}}$

The ACT111A allows dimming with a PWM signal at the DIM pin. A signal level above 1.5V enables switching and turns LED on. To turn off the LED current, the signal level has to be below 1.52V. The dimming signal frequency range is from 100Hz to 10kHz. A 200kΩ resistor is needed to connect between FB pin R_{SENSE} . A 100pF capacitor is recommended to connect from the FB pin to ground.

Key Component Selection

An inductor with RMS rating greater than load current and its saturation current at least 30% higher should be used. Inductance value is selected to make its ripple current 20-30% of the load current. A Schottky diode (D5) is usually used for better efficiency as long as the breakdown voltage can withstand the maximum output voltage. The forward current rating of the diode must be at least equal to the maximum LED current.

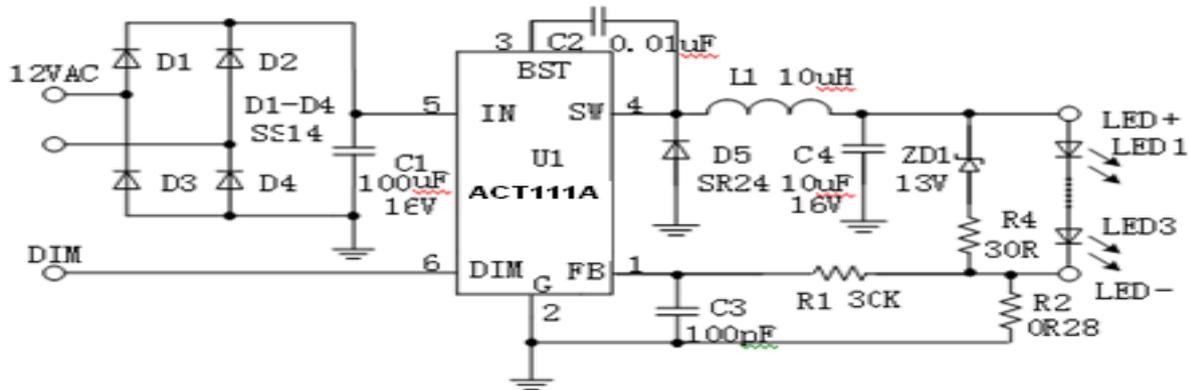
For AC input, if a conventional step-down line transformer is used, a low cost IN4001 can be used for D1-D4. However, if a high frequency electronic transformer is used, a Schottky diode such as SS14 should be used for high efficiency operation. For input and output capacitors, small size and low ESR ceramic capacitor is preferred.

PC Board Layout Guidance

Place input capacitor (C1) to IN pin, inductor (L1) and diode (D5) to SW pin as close as possible to reduce the voltage ringing at these pins. Place the current sense resistor (R2) close to FB pin. Minimize ground noise by connecting high current ground returns, the input capacitor ground lead, and the output filter ground lead to a single point (star ground configuration). There are two power loops in normal operation, one is formed when the SW is high and the high current flows through input capacitor (C1), internal MOSFET, inductor(L1), LEDs, R_{SENSE} (R2) to ground. The other loop is through inductor (L1), LEDs, R_{SENSE} (R2), ground to diode(D5). Make these loop areas as small as possible to minimize noise interaction.

ACT111A High Efficiency, Low Cost HB LED Lighting

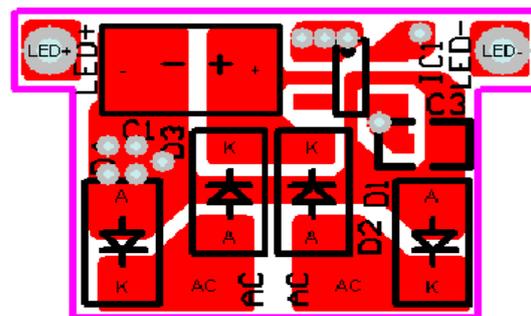
Schematic (VIN=12VDC or AC, 3x350mA LEDs)



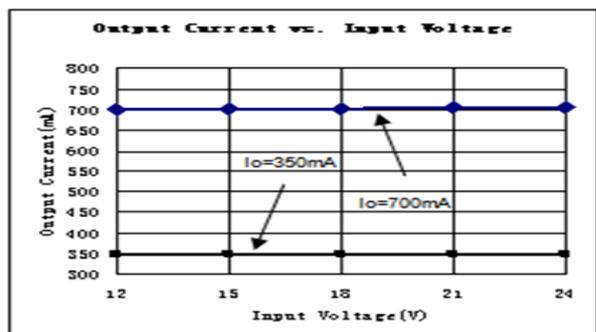
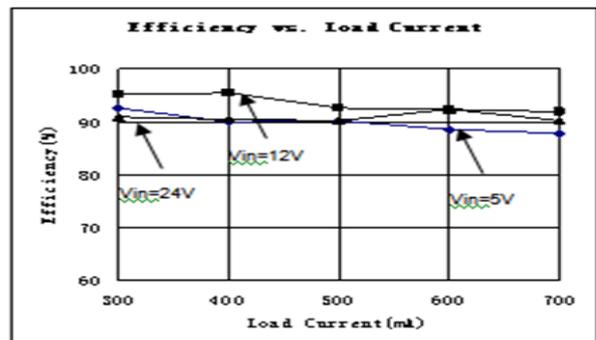
Bill of Materials

| Ref. | Description | Mftr |
|-------|---|--------|
| C1 | Capacitor Tantalum, 100uF/16V, D Case | AVX |
| C2 | Capacitor, Ceramic, 0.01uF/50V, 0603 | POE |
| C3 | Capacitor, Ceramic, 100pF/25V, 0603 | POE |
| C4 | Capacitor Ceramic, 10uF/16V, 1206 | AVX |
| D1-D4 | Diode shottky, 40V/1A, SS14, SMA | PANJIT |
| D5 | Schottky Barrier Rectifier, SR24, 40V/2.0A, SMB | PANJIT |
| ZD1 | Diode Zener, GLZ13A, 13V, 0.5W, MINI-MELF | PANJIT |
| R1 | Meter Film Resistor, 30KQ, 0603, 5% | TY-OHM |
| R2 | Meter Film Resistor, 0.28R, 1206, 1% | TY-OHM |
| R4 | Meter Film Resistor, 510Q, 1206, 5% | TY-OHM |
| L1 | SMD Power Inductor, SR0604220ML, 10uH, ±20% | QianRu |
| U1 | IC, ACT111, SOT23-6 | Active |

PCB Top Layer



Typical performance characteristics



PCB Bottom Layer

